

Developed By:
The Beach Company
211 King Street #300
Charleston, South Carolina
29401

### Owners:

Pastime Amusement, Inc. (Majority)

Mary Ellen Properties, LLC and Joyce Carolyn properties, LLC (Minority)

Project ID #: 140804-SC41-1 Revised: 10/19/14



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### 1.) Property Overview and Development Intent

The proposed Wando Village Planned Unit Development (The Property) consists of 70.37 contiguous acres located on the north side of the Wando River Bridge on SC Highway 41 (TMS #: 263-00-04-001). The Property is currently under the jurisdiction of Berkeley County and zoned as R2 - Manufactured Residential District. The majority of The Property is owned by Pastime Amusement, Inc., a subsidiary of The Beach Company, Inc. (The Developer). Mary Ellen Properties, LLC and Joyce Carolyn Properties, LLC are minority owners. This PUD Application is being submitted by The Property Owners concurrently with an Annexation application to the City of Charleston.

Currently, The Property is vacant and bounded by SC Highway 41 to the west and northwest, Tuxbury Farm Road to the northeast, and the Wando River to the south and east (See Exhibits 5-6). The Property is currently accessible from Riverbend Trail. Current conditions indicate that The Property was used as a timber tract at one time. There are a few hardwood specimens onsite that will be preserved if all possible. All development shall be subject to the specific provisions of the Tree Protection Requirements as outlined in Article 3, Part 6 of the City of Charleston Zoning Ordinance.

The wetland delineation included in the attached exhibits was conducted in 2006. A wetland delineation was also conducted for this PUD application in 2014, and The Owner is currently awaiting its approval. According to the Wetland Letter (Appendix 2), the surveyor estimates that there are approximately 2.62 acres of on-site freshwater wetlands, 6.83 acres of critical area, and 50.24 acres of highland. These figures do not include the approximately 10.7-acre critical area along the Wando River (approximately 10.7 acres). According to the 2006 survey, there are 12,330 linear feet of Critical Line on The Property of which approximately 4,800 are along the Wando River.

To ensure that The Property is developed in a comprehensive manner that incorporates open space and preserves natural features while offering a rich mix of uses and compatibility with adjacent development, The Property Owners request that PUD zoning be assigned to The Property. The PUD regulations outlined in this document will foster development that is consistent with The Property's current designation is Urban in the City of Charleston's *Century V Comprehensive Plan Update 2010* (Exhibit 2).

The intent of the PUD regulations are to create a publicly accessible Mixed-Use Village on the Wando River. The conceptual Land Use Plan illustrates the location of the two primary development pods and the permitted uses and specific requirements for each. Because the Land Use Plan (Exhibit 6) is conceptual in nature, all site plans, phasing plans, subdivision concept plans, preliminary plats, road construction plans, and final plats shall be submitted to the appropriate authority for review and approval pursuant to the provisions of this document and the City of Charleston Zoning Ordinance.

Approval of this document including the attached Land Use Plan (Exhibit 6) establishes the specific site development regulations for future development of The Property. Development of Wando Village PUD shall comply with American Disability Act (ADA) standards current at the time of development. As the community develops, input from City of Charleston staff will be incorporated into the site layout and the design of associated amenities. Unless specified otherwise within this document, all applicable City of Charleston Ordinances shall apply to the development of Wando Village.

SCDOT is currently developing plans for the reconstruction of the Highway 41 Bridge that crosses the Wando River. The PUD boundaries and circulation systems will require minor adjustments based upon the new right-of-way and roadway alignments. As illustrated in the Land Use Plan, a roundabout may be proposed for the intersection of Clements Ferry Road and Highway 41. The Owners reserve the right to adjust the circulation and the location of entrances to accommodate the roundabout if it is implemented. SCDOT approval of driveway locations and separations shall be required, and sight distance visibility at

all exits and/or intersections will be maintained in accordance with the SCDOT Access and Roadside Management Standards (ARMS) Manual.

The proposed Wando Village will be a walkable medium-density Waterfront Village offering increased public interaction with the natural beauty of the Wando River. Homes along the Wando River shall be built with regard for the context of the existing homes across the river in Dunes West. Attached Townhomes and Multi-Family Buildings are also permitted with special buffer requirements along SC Highway 41 to minimize adverse visual impacts.

### 2.) Master Plan

- a) Plat: Exhibit 3 features a Recorded Plat of the survey and wetlands as delineated in 2006. This document will be updated to reflect the 2014 wetland survey once that document is approved (See Appendix 2). The Recorded Plat includes the exact location, size, shape, gross acreage, and ownership as well as the approximate locations of all freshwater and saltwater wetlands and other critical areas.
- **b) Site Analysis:** In addition to the property line and wetland delineations in the Recorded Plat, the Site Analysis (Exhibit 4), which was also conducted in 2006, illustrates the location of existing hardwood trees and manmade features including overhead power lines, an existing structure, and an archaeological excavation site. All development shall be subject to the specific provisions of the Tree Protection Requirements as outlined in Article 3, Part 6 of the City of Charleston Zoning Ordinance.

The Property has not been surveyed for topography, but five foot contours were extracted from the US Geological Survey and are also included on the Site Analysis. Due to the extreme flatness of the site, only one 10 foot contour appears at the northernmost tip of the property, and the 5 foot contours roughly follow the OCRM critical line. Complete topographic surveys with elevations at one-foot (1') intervals based on the North American Vertical Datum of 1988 (NAVD88) will be conducted for individual sites as development occurs.

A Report on the archeological site was published in January 2007 by S&ME. In summary, the archaeological excavation is the site of a nineteenth century brickyard and borrow pit. In the report, S&ME states that excavation and data recovery efforts were sufficient to mitigate any adverse effects of development and recommends that construction be allowed to proceed without additional cultural resource investigations.

- c) Aerial Overlay: Exhibit 5 provides an overlay of the site boundary on an aerial photograph.
- **d)** Land Use Plan: Exhibit 6 is the proposed Land Use Plan that shows the locations and densities of the development pods, open space and recreational areas, and existing adjacent land uses. The plan also includes the conceptual layout for major vehicular and pedestrian circulation systems, drainage features, and proposed buffers. The Land Use Plan is intended to act as a guide and framework for development that will occur over a long period of time. Specific locations of buildings and uses, however, are subject to change and amendment during the growth and development of this property.

All new utilities serving the development will be placed underground. The developer will submit utility designs for approval by all respective utility services. A Conceptual Utility Plan is included as Exhibit 10. Letters of Coordination and existing service maps for water and sanitary sewer

service from Charleston Water System are provided in Appendix 3. All City of Charleston Fire Codes will be followed during submittals and as development occurs.

**3.) Permitted Uses by Development Pod -** Two (2) distinct development pods are indicated on the Land Use Plan. This dynamic allows for flexibility to adapt to changing market conditions while ensuring the development of an integrated, walkable, high-quality community. Specific permitted uses are as follows:

<u>Use</u>	<u>District</u>					
	Mixed-Use	Estate Lots				
Office/Professional/Medical	X					
Retail	X					
Dining/Restaurant/Bar	X					
Community Docks	X	X				
Boat Storage/Servicing	X					
Single-Family Residential	X	X				
Townhomes	X	X				
Multi-Family Residential	X					
Hotel/Bed & Breakfast	X					
Senior Living	X					

### 4.) PUD Zoning Regulations by Development Pod

a) <u>Estate Lots</u> - The design intent for the Estate Lots District is to develop Single-Family Estate Lots along the Wando River with the potential for Townhomes as well. The plan for the Estate Lots District will be carefully developed to be sensitive to the river's edge and to existing neighbors along the river. Accessory units such as granny flats are permitted on single-family lots.

Permitted Dwelling Units: single-family detached, single family attached, and townhomes.

### Dimensional Requirements:

Single-Family Detached

Minimum Lot Size: 5,000 sf Minimum Lot Width: 50' Minimum Lot Depth: 100'

Minimum Front Yard: 15' (50' for Accessory structures)

Minimum Rear Yard: 15'
Minimum Side Yard: 9'
Maximum Lot Occupancy: 60%

Maximum Building Height: 3 stories (one additional level of non-conditioned space

permitted at ground level)

Max. Fence/Wall Height: 6'

Single-Family Attached and Townhomes
Minimum Lot Size: 1,600 sf
Minimum Lot Width: 16'
Minimum Lot Depth: 100'

Minimum Front Yard: 4' (25' with front parking)
Minimum Rear Yard: 25' (35' with rear parking)

Minimum Side Yard: 20' between structures; 10' between end structure and side lot

line

Maximum Lot Occupancy: 60%

Maximum Building Height: 3 stories (one additional level of non-conditioned space

permitted at ground level)

Max. Fence/Wall Height: 6

b) <u>Mixed-Use</u> - The areas designated for Mixed-Use District Zoning offer the most convenient access to Highway 41. The proposed zoning for this district will encourage a higher density mix of uses to include retail, offices, and other commercial facilities. Multi-family housing, residential lots, and a waterfront park are also permitted in this area. For the purposes of determining specific setback and buffer requirements, buildings featuring a mix of either residential and commercial or residential and office uses shall follow the requirements of multi-family buildings or townhomes depending upon their configuration. Townhomes within the Mixed-Use district shall follow the requirements outlined in the Estate Lots section above.

<u>Permitted Dwelling Units:</u> single-family detached, single family attached, townhomes, multifamily residential, and mixed-use buildings. Densities will migrate increasingly from the Tuxbury Road Boundary towards the Wando Bridge per the District Plan shown in Exhibit 6.

### **Dimensional Requirements:**

Multi-Family Apartments

Minimum Lot Size: 1,100 sf/unit

For all Uses within the Mixed-Use District (excluding Townhomes): Front yards must meet one of the following conditions:

- i. Minimum setback and landscape buffer requirements not to include OCRM Critical Line buffers are waived where any building or structure is constructed so that a minimum of 60% of the lot frontage is occupied by a building façade that abuts the front property line provided that the primary entrance to the building is located on this façade. Building façade indentations or extensions which are part of the building's architectural design shall count toward the minimum 60% lot frontage requirement. On a corner lot, the building façade shall occupy at least 60% of the frontage on the primary street and no less than 25% on the secondary street. Additionally, a secondary entrance must be located on the secondary street facade. On a corner lot, the abutting building frontages must extend to the corner or have a corner entrance in which case the primary and secondary entrance requirements are waived. Service entrances may not count toward the primary, secondary, or corner entrance requirements. Stoops and open porches, bay windows, and balconies may extend up to 4 feet into the right-of-way, with an encroachment permit from the City, provided at least 5 feet of clear sidewalk passage remains. Stoops and open porches, bay windows, and balconies may extend up to 7 feet into a front set-back zone. Loading docks, service areas, and trash disposal facilities shall not face streets, parks, squares or significant pedestrian spaces.
- ii. Where the conditions of (i) are not met, the minimum front yard depth for all structures is ten (10) feet;

### Minimum Side and Rear Yard:

10' shall be required along each rear and side lot line; except that where a firewall meeting the standards of the current edition of the city's building code is constructed at the property line; the side or rear yard requirement may be waived along the respective side or rear lot line.

### Maximum Building Height:

3 stories with one additional level of non-conditioned space permitted at the ground level. All local building codes applicable at the time of construction must be met with regard to fire ratings, fire exits, and all other requirements in the current International Building Code.

Minimum Building Height: 1.5 stories
Maximum Lot Occupancy: 90%

c) <u>Parking Requirements</u> – Except as noted below, parking is to be provided for all uses per the City of Charleston Zoning Ordinance standards current at the time of development. Within all districts, parking may be located under buildings. Parking structures and shared parking areas are allowed so long as they comply with the ULI standards for shared parking. In any off-street parking lot, no more than 10 consecutive parking spaces are permitted without a landscape island. Each island is to be planted with a minimum of 1 canopy tree as well as ground cover and/or shrubs. Islands are to be protected with a 6" barrier constructed of raised concrete curbing or equivalent materials.

### Mixed-Use/Commercial

Dining/Restaurant/Bar 1/200 sf, plus ½ for each staff

Multi-Family Residential1.5/unitRetail1/250 gross sfOffice/Professional/Medical1/300 sf

Residential

Multi-Family Residential 1.5/unit Townhome 1.5/unit

Single-Family 2/home (off street)

### 5.) Open Space and Recreational Areas

The Land Use Plan indicates several areas to be dedicated as open space to serve the recreational needs of people living in, working in, and visiting Wando Village while engaging them with adjacent natural resources. Conceptually, the usable open spaces may incorporate walks, ponds, pervious paths, pools, buffers, trails, seating, lighting, and plantings. The pervious paths may be placed within designated access easements on private property within the critical line buffers so long as they are set back a minimum of 20 feet from the OCRM Critical Line. Exceptions to the 20-foot setback are permissible to provide access to water dependent structures. Pedestrian paths will connect the Estate Lots District to the Mixed-Use areas which will feature a series of accessible parks. The waterfront park will offer extensive views and allow users to directly engage with the Wando River and its marshes. All open space and recreational areas outside of the public right-of-way will be owned and maintained by the Property Owners Association (POA) as described in Section 9 of this document. Upon completion, all portions of the Wando Village PUD will be connected through ADA accessible pedestrian paths or sidewalks. See the Land Use Plan (Exhibit 6) for open space requirement calculations and locations. Within each development phase, all open space amenities will be constructed prior to final plat approval.

### 6.) Landscape and Buffer Requirements

In addition to the buffers outlined below, a 100' undisturbed buffer shall be maintained along the northern property line abutting Tuxbury Farm Road. The following Buffer Types refer to the City of Charleston Zoning Ordinance designations. Please refer to the City of Charleston Zoning Ordinance for buffer specifications. Landscape material used for buffer and accent planting should emphasize native materials. All materials, sizes, and spacing shall conform to the standards set forth in the City of Charleston Zoning Ordinance:

Between any use and Highway 41: Type C Buffer (average width of 25', not to go below 15').

Wherever a multi-family building (excluding townhomes), mixed-use building, or any nonresidential use is proposed for a site or lot adjoining a single-family or townhome lot: Type B Buffer (minimum width of 15').

Buffer plantings must be planned so as to screen between uses and provide a visual barrier. Existing plants may count toward buffer requirements so long as they fulfill all requirements of this section and all City of Charleston landscape and buffering requirements. Buffers shall be located along the perimeter of a lot or parcel and shall extend to the boundary line of the lot or parcel. Buffers shall not be located on any portion of an existing public or private street right-of-way. Where utility or drainage easements exist along property lines, the buffer shall be located adjacent to the easement and may be reduced by the width of the easement on the property where the buffer is required or twenty-five percent (25%) of the required buffer width, whichever is smaller.

Street trees are to be planted along all roadways according to City of Charleston Subdivision regulations (Article 8, Part 4, Section 54-831(e)).

Along OCRM Critical Lines, the following buffers apply:

### Estate Lots & Mixed-Use Areas

Type L Buffer (minimum 20' width; see City of Charleston Zoning Ordinance, Article 3, Part 8, Section 54-347 and 54-348)

10' building setback from the buffer line

### POA Land

Limited removal of vegetation within the OCRM buffer on POA land is permissible for views and access to water dependent structures, subject to POA guidelines. Approved boat ramps and docks, appurtenant access facilities, and other publicly accessible uses such as concessions, public yachting facilities, and civic and recreational facilities may be installed within this buffer within POA lands. Any removal of a grand tree within these buffers will require mitigation as specified in the City of Charleston Zoning Ordinance (Article 3, Part 6, Sections 54-325 through 54-339).

### 7.) Traffic Impact Study

Appendix 1 is a Traffic Impact Analysis prepared for the Beach Company based upon the proposed Wando Village PUD. The document is still considered to be in draft form until it is reviewed and approved by both the City of Charleston and SC Department of Transportation. Revised versions of the Traffic Impact Analysis will be submitted to the City of Charleston as they develop. Approval of the PUD does not guarantee approval of the traffic impact study as submitted. The City of Charleston Traffic and

Transportation Department (or SCDOT if SCDOT roads are impacted) has the final authority to approve site related traffic impacts and mitigation. Additional traffic impact analyses may be required on a per site/project basis if the proposed impacts are determined to be outside of the original scope of the PUD.

### 8.) Drainage Basin Analysis

All land within the PUD drains directly into the upper reaches of the Wando River as shown in Exhibit 8: Regional Watershed Map. The Wando River outlets into the Cooper River which flows directly into Charleston Harbor. As shown in Exhibit 9: Storm Drainage Patterns, current storm drainage either sheet flows directly into the Wando River (indicated by yellow arrows), or follows one of three other flow patterns that also discharge into the Wando River via tidal creeks. As shown on the Land Use Plan, approximately 5 acres of The Property will be devoted to stormwater retention. The stormwater drainage system will be designed to conform to the City of Charleston Stormwater Design Standards Manual and other State regulatory agency standards to ensure that development meets all stormwater discharge quality and quantity requirements. Any new topo surveys will be 1' intervals based on NAV88 datum.

### 9.) Density

The Wando Village PUD application proposes to maintain its current allowable density range of 8-12 units/acre. According to the 2014 draft wetland survey, the Property contains approximately 52.86 acres of highland including freshwater wetlands; the maximum build-out is 420 units.

### 10.) Rights-of-Way

The Wando Village PUD is limited to four points of ingress/egress along SC Highway 41. Approximate locations of these access points are shown in Exhibit 6; however, spacing will be adjusted according the proposed development, the proposed Highway 41 realignment, and SCDOT encroachment permits. SCDOT approval will be required for all driveway locations, and sight distance visibility at all exits and/or intersections will be maintained in accordance with the SCDOT Access and Roadside Management Standards (ARMS) Manual. The City of Charleston Department of Traffic & Transportation has the final authority to approve site related traffic impacts and mitigation. Additional traffic impact analyses may be required on a per site/project basis if the impact is determined to be outside of the original scope of the PUD.

See Exhibit 7 for typical cross sections proposed for internal roadways in Wando Village. All roads within the PUD are anticipated to be public and constructed in accordance with accepted engineering standards. Public and private roadway designs will apply civil design software to check the adequacy, maneuverability, and safety of all proposed sections and geometrics. Within the mixed-use area, plans will strive to create a grid of streets and blocks. While encouraged where feasible, on-street parking shall only be permitted in designated parking areas within the public right-of-way. Sidewalks or trails are to be provided along all roadways within the PUD for pedestrian access. Street lights are to be required in all public rights-of-way as per City of Charleston ordinances.

Other than occasional deliveries, heavy truck traffic will be prohibited within the development. No container storage or trailer stacking will be allowed. Overnight parking of eighteen-wheel vehicles is strictly prohibited.

### 11.) Property Owners Association and Design Review

Ownership and maintenance of all common open space areas not included in the public right-of-way shall be the responsibility of the Property Owners Association (POA). Such responsibilities include, but are not

limited to, landscaping, parking stalls, pedestrian paths, drainage, lighting, ponds, and private utilities. The Subdivision Concept Plan will outline the construction of these pedestrian paths, parks, and other open spaces. POA amenity areas are required to receive City of Charleston Technical Review Committee (TRC) review and approval, except for mail kiosks and tot lots.

Membership in the POA will be open to all persons having ownership of properties within the PUD. The POA will be managed by The Developer (or its designated representative) collecting all fees and handling POA responsibilities until such time that over one-half of the total developable land within the PUD is sold, at which time duties will be turned over to a successor chosen by the POA. A POA Board of Directors will be created to represent both the commercial and residential sections of the development. A declaration of covenants, conditions, and restrictions shall outline the specific responsibilities of the POA and shall run with the land.

Amenity space will be dedicated for uses such as a community pool and parks to serve the residential portion of the development. The initial phase of construction of these features will be the responsibility of The Developer until the POA is established. Within each development phase, all open space amenities will be constructed prior to final plat approval. Upon project completion, the POA is responsible for connecting any gaps in pedestrian connectivity as outlined in the POA declaration of covenants, conditions, and restrictions.

The Developer and POA reserve the right to establish and enforce Design Guidelines and/or a designated review board to review and approve all elements of building and site design. The POA and/or its designee shall have reasonable authority to approve all aspects of site planning, landscape and exterior architecture to include aesthetic appropriateness, environmental implications, traffic impacts and any other site specific matters not delineated.

All non-residential buildings that abut the required buffer along SC Highway 41 shall be required to follow the City of Charleston Design Review Board (DRB) review and approval process.

### 12.) Signage

One 'master' development sign shall be allowed within the required buffer at each entry point along SC Highway 41. Such signs shall be monument style and will require DRB review and approval. Additionally, one 'master' developer sign shall be allowed for residential developments at each entry point along internal PUD roads. Such signs shall be monument style and will require POA review and approval.

All directional and traffic signage shall conform to the Manual on Uniform Traffic Control Devices (MUTCD) Standards.

### 13.) Anticipated Phasing

While still conceptual in nature, it is anticipated that initial development will occur in the portion of the Mixed-Use District along the Wando River to be followed by the Estate Lots District and, finally, by the northern portion of Mixed-Use District . Timelines and the order of development are subject to change depending upon SC Highway 41 realignment projects and market conditions. Model Homes and certain amenities may start construction prior obtaining the final plat.

## **EXHIBITS**



# WANDO VILLAGE PUD OWNER: PASTIME AMUSEMENT, INC. DEVELOPER: THE BEACH COMPANY





EXHIBIT 1: EXISTING ZONING OF SUBJECT & ADJACENT PARCELS (BERKELEY COUNTY)

N.T.S. **EX. 1** 

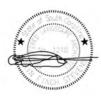
# **EXHIBIT 2: LAND USE - UPPER CAINHOY**

FROM: CENTURY V: 2010 COMPREHENSIVE PLAN UPDATE
August 25, 2014

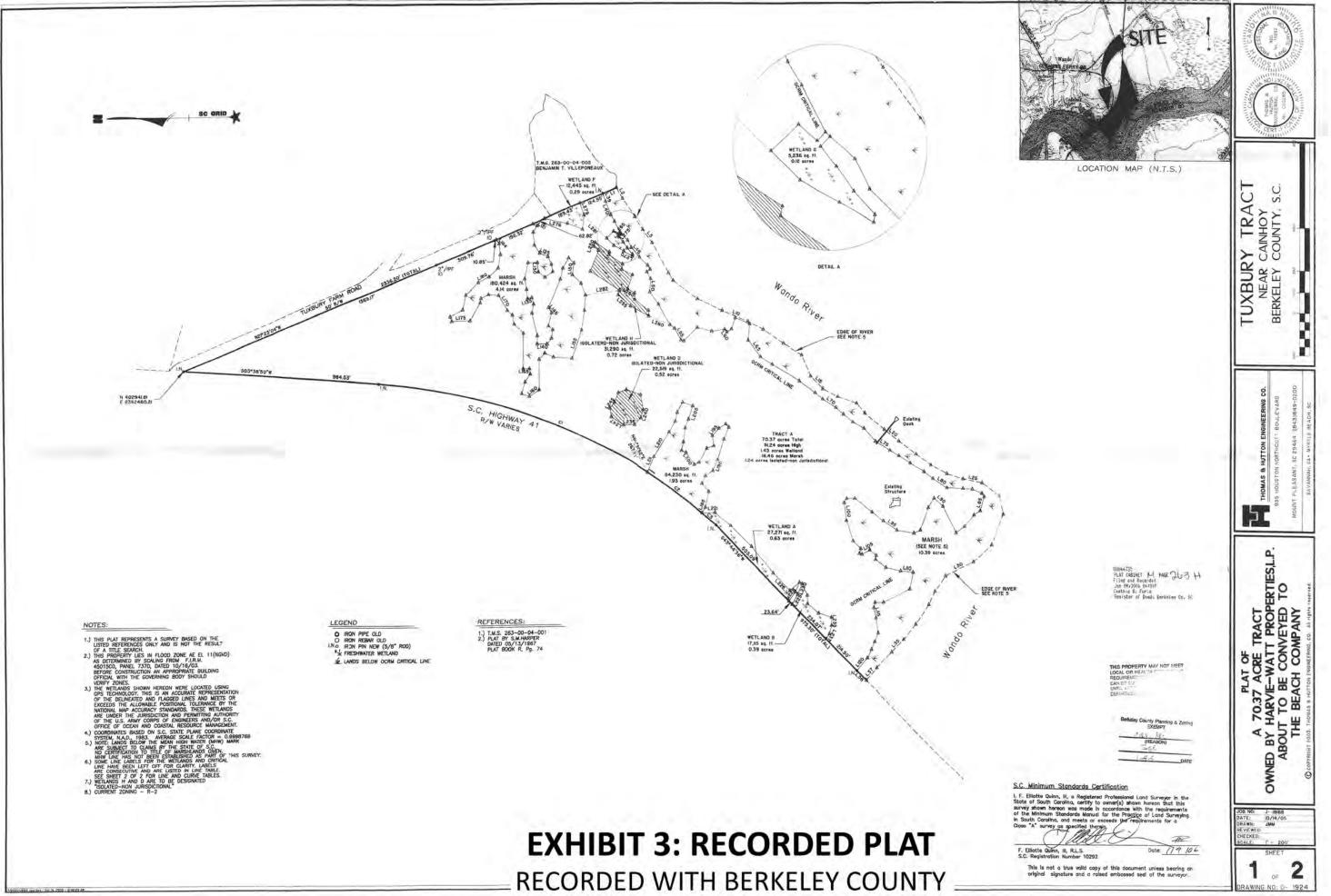


WANDO VILLAGE PUD OWNER: PASTIME AMUSEMENT, INC. DEVELOPER: THE BEACH COMPANY





**EX. 2** 



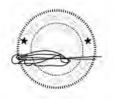
WANDO VILLAGE PUD OWNER: PASTIME AMUSEMENT, INC. DEVELOPER: THE BEACH COMPANY

**EX. 3** 



# WANDO VILLAGE PU OWNER: PASTIME AMUSEMENT, INC. DEVELOPER: THE BEACH COMPANY





EX. 4

300'

Scale: 1"=300'

600'

# **EXHIBIT 4: SITE ANALYSIS & TOPOGRAPHY**

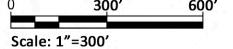


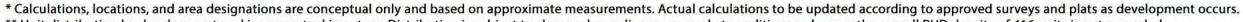
# WANDO VILLAGE PUD OWNER: PASTIME AMUSEMENT, INC. DEVELOPER: THE BEACH COMPANY

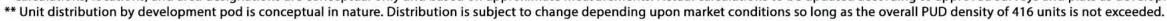
DAVIS & FLOYD, INC. No. C00538 P. COMPANY CONTRACTOR AUTHORITIES OF AUTHORITIES O



# **EXHIBIT 5: AERIAL OVERLAY**

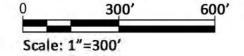








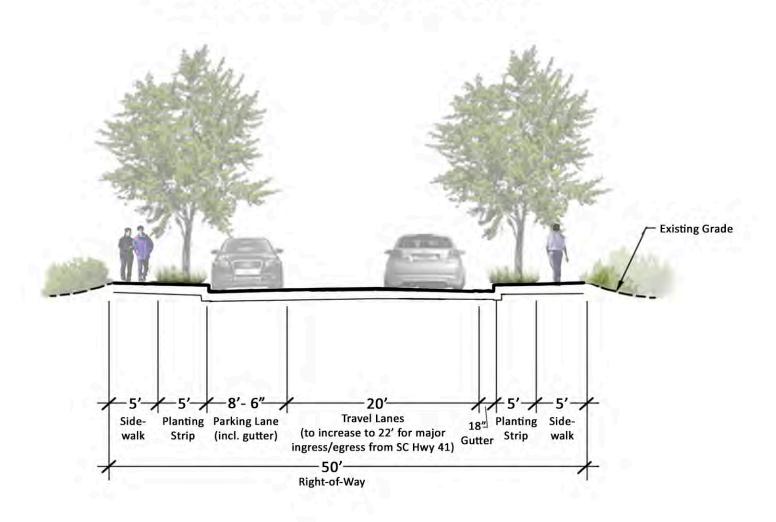
# **EXHIBIT 6: LAND USE PLAN**



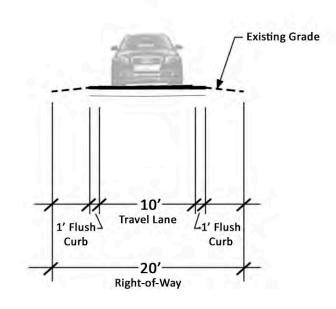
**EX.** 6

WANDO VILLAGE PUD OWNER: PASTIME AMUSEMENT, INC. DEVELOPER: THE BEACH COMPANY

# Two way traffic; Parking on one side in designated parking areas only. **Vertical Curb.** Sidewalk and Plantings both sides.\*



# Internal alleys; One way traffic. Flush Curb.\*



<sup>\*</sup> Typical sections conceptual only. Actual roadway designs to vary based on site conditions and need. All public ROWs to feature street lights as per City of Charleston ordinances current at the time of design.





# **EXHIBIT 8: REGIONAL WATERSHED MAP**

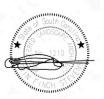
COOPER RIVER

SITE

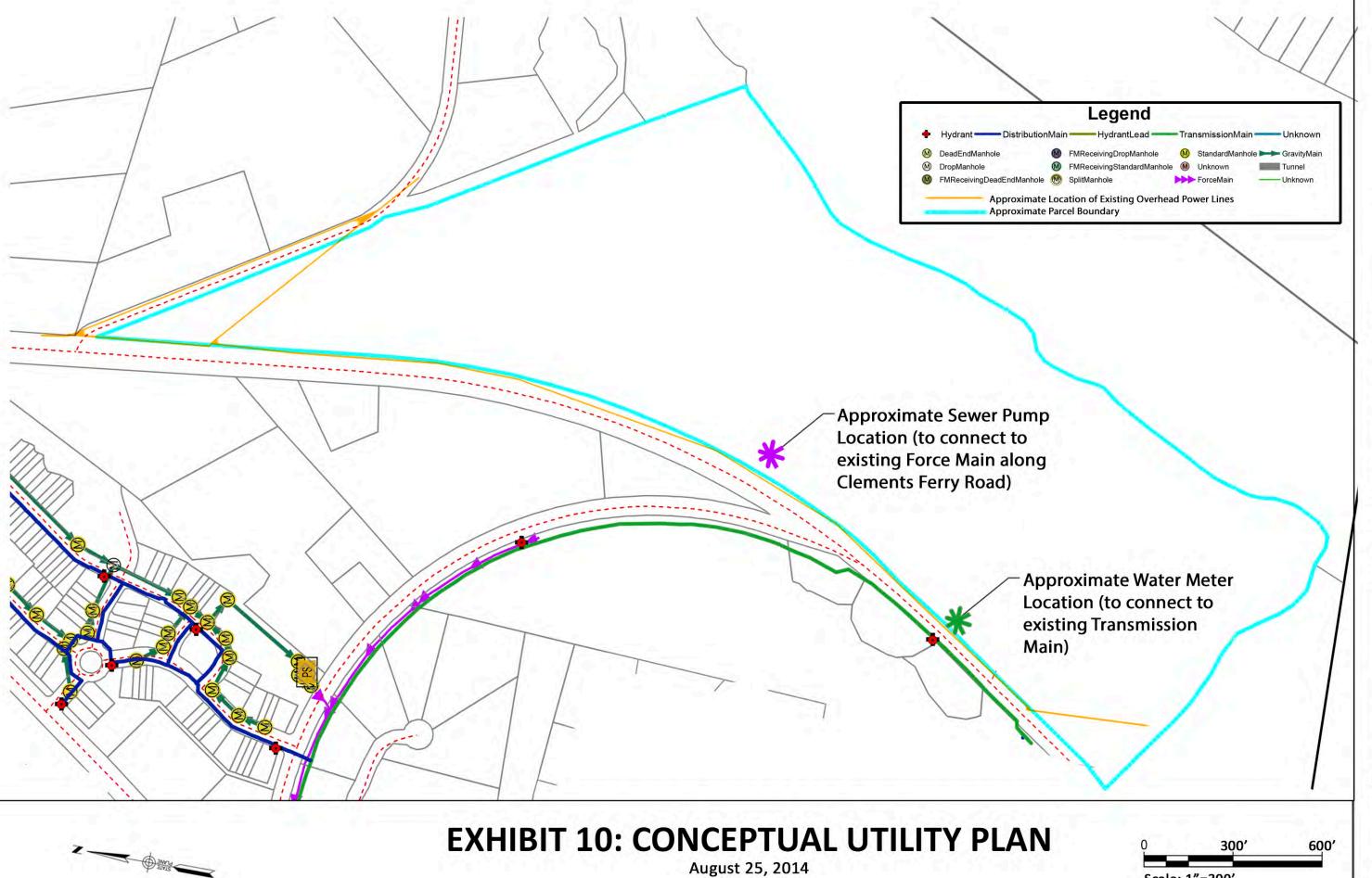
WANDO RIVER

UPPER WANDO RIVER
WATERSHED

UPPER WANDO RIVER WATERSHED



# **EXHIBIT 9: STORM DRAINAGE PATTERNS**



DAVISEngineering
Architecture

WANDO VILLAGE
OWNER: PASTIME AMUSEMEN
DEVELOPER: THE BEACH COME





Scale: 1"=300'

## **APPENDICES**

## APPENDIX 1

### **Traffic Impact Analysis**

# Wando Village

Draft Report - July 2014

# THE BEACH COMPANY

REAL ESTATE DEVELOPMENT • SALES • LEASING • MANAGEMENT

Building Traditions Since 1945

Traffic Impact Analysis Wando Village D&F Job No. 31573.00.

Prepared for:

Charles S. Way, Jr.
Chairman
The Beach Company, Inc.
211 King St #300
Charleston, SC 29401

Prepared by:

Davis & Floyd, Inc. 3229 West Montague Avenue North Charleston, SC 29419 [843] 554 8602







### INTRODUCTION

As requested, Davis & Floyd, Inc. has conducted an analysis to assess the traffic impacts associated with the new development referred to as "Wando Village" in Charleston, South Carolina. The proposed Wando Village development will be located on the north side of the Wando River Bridge on SC Highway 41 and is expected to include the construction of 35 single family homes, 565 apartment units, 15,000 sf of restaurant space, and 10,000 sf of retail space. Access to the Wando Village will be provided by three access drives along SC 41 north of the future Clements Ferry Rd/SC 41 intersection and one access drive along SC 41 south of the future Clements Ferry Rd/SC 41 intersection. The development will be constructed in phases and is anticipated to be complete and fully operational in a 7 year period, depending on market conditions.

### **EXISTING CONDITIONS**

### **Project Study Area:**

The study area for this project includes the following three intersections located along/near SC Highway 41.

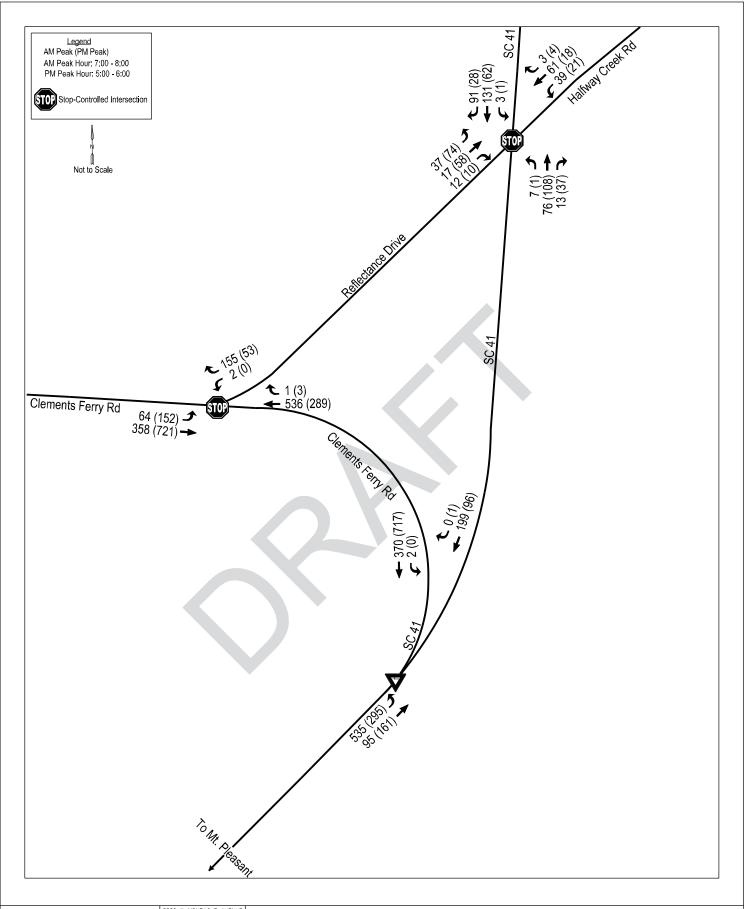
- SC 41 / Clements Ferry Road
- SC 41 / Halfway Creek Road
- Clements Ferry Road / Reflectance Drive

### **Existing Intersection Geometry:**

Detailed field reviews of the area were conducted in April, 2014. These reviews included site visits to document the existing roadway geometry and intersection traffic control devices as well as conducting traffic turning movement counts for the morning (6:30 AM - 8:30 AM) and PM (4:00-6:00) peak hours at the intersections. A summary of the traffic count data obtained at these locations is provided in **Figure 1**. The existing roadway conditions are summarized as follows:

### • SC 41 / Clements Ferry Road:

The intersection of SC 41 / Clements Ferry Road is a three-way un-signalized intersection with SC 41 making up the northbound and southbound approaches and Clements Ferry Road making up the eastbound approach. The northbound and southbound approaches of SC 41 consist of a single approach lane from which all movements are made. The eastbound approach of Clements Ferry Road consists of a single approach lane from which all movements are made. The Clements Ferry Road approach is controlled by a yield sign and the SC Highway 41 approaches are free-flow. The posted speed limit along this segment of SC Highway 41 is 35 mph and Clements Ferry Road is posted at 35 mph.



DAYIS Engineering Architecture
FLOYD Environmental
Laboratory Services
GREENWOOD: CHARLESTON . COLUMBIA

FIGURE 1

# 2014 Existing Peak Hour Traffic Volumes

SC 41 / Clements Ferry Rd / Reflectance Dr Charleston, South Carolina

### • SC 41 / Halfway Creek Road:

The intersection of SC 41 / Halfway Creek Road is a four-way un-signalized intersection with SC 41 making up the northbound and southbound approaches, Reflectance Drive making up the eastbound approach, and Halfway Creek Road making up the westbound approach. The northbound and southbound approaches of SC 41 consist of a single approach lane from which all movements are made. The eastbound approach of Reflectance Drive and westbound approach of Halfway Creek Road consist of single approach lanes from which all movements are made. The Reflectance Drive and Halfway Creek Road approaches are controlled by a stop sign and the SC Highway 41 approaches are free-flow. There are flashing beacons on each approach. The posted speed limit along SC Highway 41 Road is 45 mph, the posted speed limit on Halfway Creek Road is 55 mph and the speed limit on Reflectance Drive is 40 mph.

### Clements Ferry Road / Reflectance Drive

The intersection of Clements Ferry Road / Reflectance Drive is a three-way unsignalized intersection with Clements Ferry Road making up the eastbound and westbound approaches, and Reflectance Drive making up the southbound approach. The eastbound and westbound approaches of Clements Ferry Road consist of a single approach lanes from which all movements are made. The southbound approach of Reflectance Drive consists of a single approach lane from which all movements are made. The Reflectance Drive approach is controlled by a stop sign and the Clements Ferry Road approaches are free-flow. The posted speed limit along this segment of Clements Ferry Road is 35 mph and Reflectance Drive is 40 mph.

### **Existing Traffic Operations:**

The Level-of-Service (LOS) analysis is used to provide an evaluation of the overall operational conditions within the traffic stream. The LOS is defined in the Transportation Research Board's *Highway Capacity Manual* as a "qualitative measure describing operational conditions within a traffic stream, based on service measures such as speed, travel time, freedom to maneuver, traffic interruptions, comfort, and convenience." Six LOS categories have been defined and given letter designations from "A" to "F" with "A" representing the best operational conditions (minimal interruptions, good progression) and "F" representing the worst conditions (severe congestion, slow travel speeds). A summary of the delay associated with each LOS is summarized in Table 1. Acceptable intersection service levels are generally considered to be LOS "D" or better.

<sup>1.</sup> Highway Capacity Manual, p. 5-8, Transportation Research Board, National Research Council, Washington, D.C. 2000

TABLE 1 Intersection Delay and LOS

Level of Service	Un-signalized Intersection Average Control Delay (seconds/vehicle)	Signalized Intersection Average Control Delay (seconds/vehicle)
Α	0 - 10	≤10
В	>10 - 15	>10 – 20
С	>15 - 25	>20 – 35
D	>25 - 35	>35 – 55
E	>35 – 50	>55 – 80
F	>50	>80

In order to assess the overall performance of the existing intersections, a LOS analysis has been performed using SYNCHRO Studio 7 traffic modeling software. The results of this analysis are provided in Table 2.

TABLE 2
Existing Traffic Conditions

	2014 – Existing Traffic Conditions								
Un-signalized Intersections		AM Peak Ho	our	PM Peak Hour					
	LOS	Delay	V/C	LOS	Delay	V/C			
SC 41 / Clements Ferry Road <sup>1</sup>	С	19.2	0.46	С	17.5	0.29			
SC 41 / Halfway Creek Road <sup>1</sup>	В	13.8	0.26	В	13.4	0.32			
Clements Ferry Road / Reflectance Drive <sup>1</sup>	С	17.8	0.44	В	10.4	0.09			

<sup>1</sup> LOS/ Delay/ V/C shown for the critical intersection approach

As indicated in Table 2 above, each of the study area intersections are operating at acceptable levels (LOS D or better) for both the AM and PM Peak traffic hours.

### 2021 "NO-BUILD" CONDITIONS

### Area Growth Rate:

In order to assess the baseline traffic conditions expected for the 2021 project horizon year, historic traffic volumes were reviewed for both Clements Ferry Road and SC Highway 41 (SCDOT count stations #198 and #269) over the past 7 years. It was determined that the roadways have collectively experienced a negative annual growth. However, in order to provide a conservative analysis for future growth, a 1.0% annual growth rate was utilized to develop 2021 No Build traffic volumes. The historic traffic volumes and annual growth rates are provided in Table 3.

TABLE 3
Background Growth Rate

Station	Road	Location	2005	2012	% annual Growth	Use
198	SC 41	Joe Rouse Rd to Berk. Co. Line	13,500	12,100	-1.55%	1%
269	Clements Ferry	SC 41 to Jack Primus	15,500	14,800	-0.66%	1%

### 2021 "No-Build" Analysis:

A level-of-service analysis has been conducted to assess the anticipated roadway conditions during the 2021 project horizon year. The traffic volumes assumed for this analysis include the conservative 1% annual growth in background traffic. It should be noted, that the SC 41 / Clements Ferry Road intersection geometry and location is currently being improved by the SCDOT. Preliminary SCDOT plans for the "S.C. Route 41 Bridge Replacement over Wando River" project provided by ICA Engineering show the new intersection north of its current location. The existing intersection will be converted to a "tee" type intersection where the Clements Ferry Road eastbound approach and SC 41 northbound approaches will be aligned as the "through" movements and the SC 41 southbound approach will be a side street approach. The northbound approach of SC 41 will include a right turn lane and a through lane. The future intersection will be signalized. These improvements have been reflected in the analysis for the 2021 "No-Build" traffic conditions. The traffic volumes associated with the 2021 "No-Build" conditions are summarized in Figure 2. The results of this analysis are provided in Table 4.

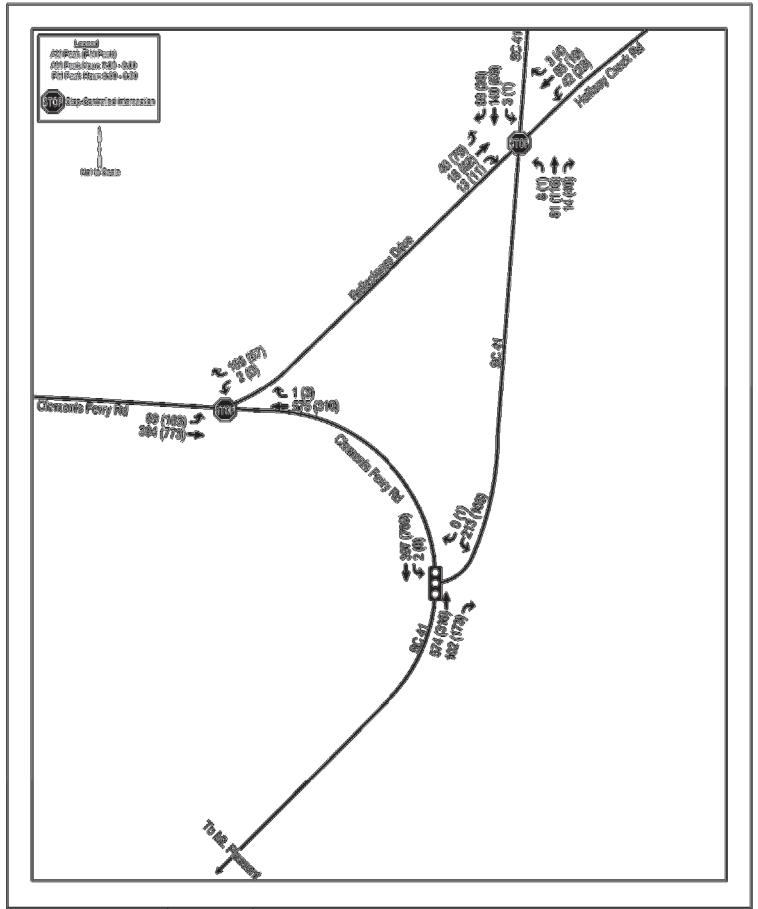
TABLE 4
2021 "No-Build" Traffic Conditions

	2021 – "No-Build" Traffic Conditions						
Signalized Intersections	AM Peal	k Hour	PM Peak Hour				
	LOS	Delay	LOS	Delay			
SC 41 / Clements Ferry Road <sup>1</sup>	В	10.4	Α	7.8			
SC 41 / Halfway Creek Road <sup>2</sup>	В	15.0	В	12.2			
Clements Ferry Road / Reflectance Drive <sup>2</sup>	С	20.1	В	10.7			

<sup>1.</sup> LOS / Delay shown for the overall intersection operation

As indicated above, each of the study area intersections is expected to operate at acceptable service levels (LOS D or better) for the 2021 "No-Build" traffic scenario.

<sup>2</sup> LOS/ Delay shown for the critical intersection approach



VIS Engineering
Architecture
Environmental

FIGURE 2

2021 "No-Build" Peak Hour Traffic Volumes

SC 41 / Claments Ferry Rd / Reflectance Dr Charleston, South Carolina

### PLANNED DEVELOPMENT

### **Site Development and Access:**

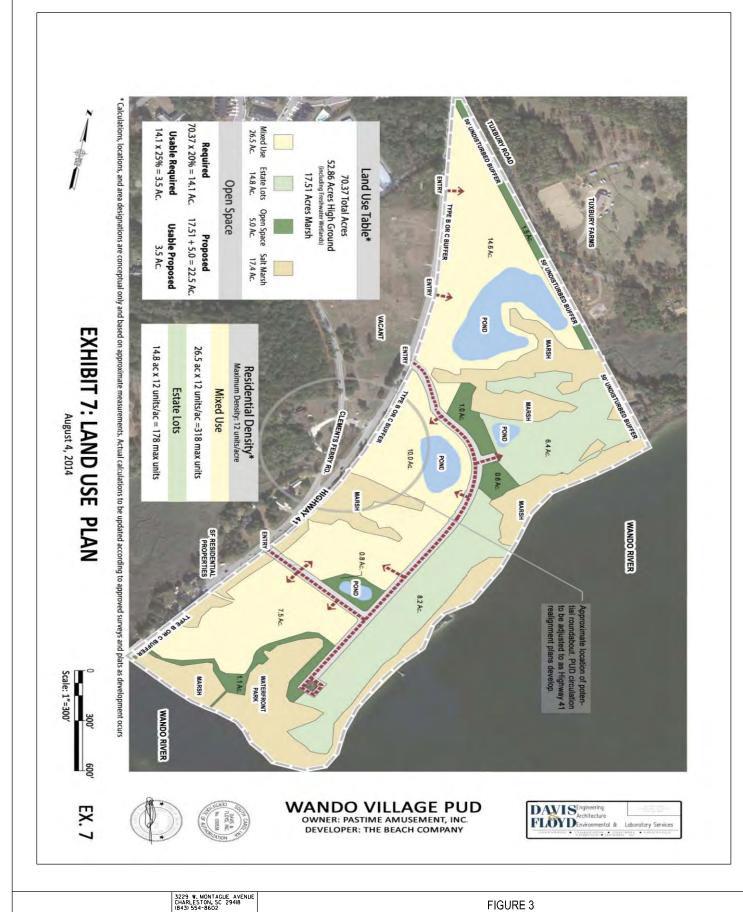
The proposed Wando Village is expected to include the construction of 35 single family homes, 565 apartment units, 15,000 sf of restaurant space, and 10,000 sf of retail space. Access to Wando Village will be provided by three access drives along SC 41 north of the future Clements Ferry Rd/SC 41 intersection and one drive along SC 41 south of the future Clements Ferry Rd/SC 41 intersection. A conceptual site plan for the development is provided in **Figure 3**.

### **Trip Generation:**

In order to estimate the traffic that could be expected for this development, the trip generation rates provided in the *Trip Generation Manual*, 9<sup>th</sup> *Edition*, published by the Institute of Transportation Engineers were applied to the proposed land uses in order to estimate the total site traffic. ITE Land Use Codes #210 (Single Family Detached Housing), #222 (High-Rise Apartment), #826 (Specialty Retail Center), and #932 (High-Turnover (Sit Down) Restaurant), were used to predict the site traffic for this multi-use facility. Due to the retail nature of the development, internal and pass-by capture was also considered in the trip generation estimates. Internal capture considers interaction between multiple uses in a development and pass-by traffic is attracted from the existing traffic volumes on adjacent roadways and reduces the new trip impacts of a retail project site. Internal and pass-by capture was estimated using information contained in ITE's Trip Generation Handbook, 2<sup>nd</sup> Edition (2004) reference. A summary of the expected traffic volumes are provided in Table 5.

TABLE 5
Site Trip Generation

Land Use	ITE LUC	Scale	Weekday			Weekday AM Peak Hour			Weekday PM Peak Hour		
Land OSE			Inbound	Outbound	Total	Inbound	Outbound	Total	Inbound	Outbound	Total
Single Family	210	35 lots	200	200	400	9	26	34	26	15	41
Apartment	222	565 units	1172	1172	2344	42	127	170	118	75	193
Restaurant	932	15,000 sf	954	954	1907	89	73	162	89	59	148
Retail	826	10,000 sf	233	233	465	79	86	165	20	25	45
Gross Trips:		2559	2559	5116	219	311	531	252	175	427	
-Internal Capture Trips:								-6	-5	-11	
-Pass-by Capture Trips:								-38	-25	-63	
New, External Trips:		2559	2559	5116	219	311	531	209	145	353	



Wando Village Conceptual Site Plan

Wando Village Charleston, South Carolina

IS Engineering
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Environmental
Laboratory Services CREENWOOD • CHARLESTON • COLUMBIA S O U T H C A R O L I N A

### **Trip Distribution:**

The trip distribution pattern for the proposed Wando Village is based on the existing traffic patterns observed on the surrounding roadways. Based upon this information, the general distribution of new project trips was assumed to be:

- 45% to/from Clements Ferry
- 35% to/from Mt. Pleasant
- 20% to/from SC 41 relocated

### 2021 Build Traffic Conditions:

In order to assess the impacts of this development at full build-out in 2021, the 2021 "No-Build" traffic volumes were combined with the trip generation projections and the trip distribution patterns to develop the 2021 "Build" traffic volumes. The anticipated 2021 "Build" traffic volumes are shown in **Figure 4**. The study area intersections were then analyzed to determine the impacts of the additional site traffic. A summary of the analysis for the 2021 "Build" traffic conditions is provided in Table 6.

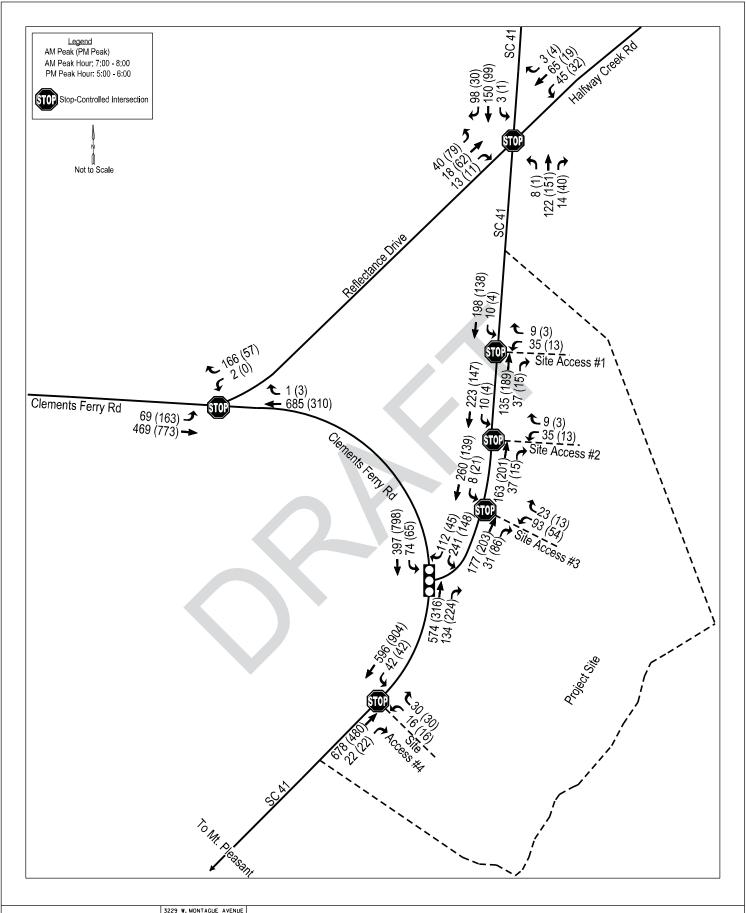
TABLE 6
2021 Build Traffic Conditions

	2021 – "Build" Traffic Conditions					
Intersections	AM Pe	ak Hour	PM Peak Hour			
	LOS	Delay	LOS	Delay		
SC 41 / Clements Ferry Road <sup>1</sup>	В	18.7	В	11.6		
SC 41 / Halfway Creek Road <sup>2</sup>	В	14.2	В	13.3		
Clements Ferry Road / Reflectance Drive <sup>2</sup>	С	22.0	В	10.7		
SC 41 / Site Access #12	В	11.2	В	10.7		
SC 41 / Site Access #22	В	11.7	В	10.9		
SC 41 / Site Access #32	В	12.9	В	12.0		
SC 41 / Site Access #42	С	15.2	В	14.4		

<sup>2.</sup> LOS / Delay shown for the overall intersection operation

As indicated in the level-of-service analysis, each of the study area and site access intersections is expected to operate at acceptable service levels (LOS D or better) for the 2021 "Build" traffic scenario.

<sup>3</sup> LOS/ Delay shown for the critical intersection approach



DAVIS Engineering Architecture
FLOYD Environmental
Laboratory Services
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FIGURE 4

# 2021 "Build" Peak Hour Traffic Volumes

SC 41 / Clements Ferry Rd / Reflectance Dr Charleston, South Carolina

### **RECOMMENDATIONS / CONCLUSIONS**

The traffic volumes associated with the construction of the Wando Village are not expected to have a significant impact on the surrounding roadway network. As indicated in this analysis, the 2021 "Build" traffic conditions at all of the study area and site access intersections are expected to operate at acceptable service levels (LOS D or better).

In order to address the impacts directly associated with the Wando Village project, the following intersection improvements are recommended:

### SC 41 / Site Access #1:

 Construct a single turn lane from which all movements are made for the outbound approach and one lane for the inbound approach of site access #1.

### SC 41 / Site Access #2:

O Construct new single turn lane from which all movements are made for the outbound approach and one lane for the inbound approach of site access #2.

### • SC 41 / Site Access #3:

 Construct a right turn lane (150' storage / 150' taper) and left turn lane for the outbound approach and one lane for the inbound approach of site access #3.

### SC 41 / Site Access #4:

 Construct a right turn lane (150' storage / 150' taper) and left turn lane for the outbound approach and one lane for the inbound approach of site access #4.

The site access locations used in this analysis were based on a conceptual site plan provided by the client and preliminary roadway design plans provided by ICA Engineering. The site access locations will need to be coordinated with and approved by the SCDOT to ensure they complement the planned roadway improvements along SC 41 and Clements Ferry Road.

# APPENDIX A Traffic Counts

735 Maryland St. Columbia, SC 29201

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% Bank 2 11.1

0.2

File Name: SC 41 @ Halfway Creek Rd

Site Code : 00043014 Start Date : 4/30/2014

					(	Groups P	rinted- U	nshifted -	- Bank 1	- Bank 2							
		SC ·	41			alfway C				SC -	41		Н	alfway C	creek Rd		
		Southb	ound			Westb	ound			Northb	ound			Eastbo	ound		
Start Time	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Int. Total
06:30	1	41	22	0	16	20	0	0	1	4	2	0	15	5	1	0	128
06:45	1	43	20	0	15	15	0	0	2	13	1	0	7	4	2	0	123
Total	2	84	42	0	31	35	0	0	3	17	3	0	22	9	3	0	251
07:00	1	26	15	0	13	17	1	0	1	17	2	0	7	4	5	0	109
07:15	1	35	22	0	14	11	1	0	0	19	4	0	9	2	1	0	119
07:30	1	35	31	0	6	20	1	0	6	18	5	0	8	6	4	0	141
07:45	0	35	23	0	6	13	0	0	0	22	2	0	13	5	2	0	121
Total	3	131	91	0	39	61	3	0	7	76	13	0	37	17	12	0	490
08:00	0	38	13	0	9	15	0	0	1	12	6	0	9	6	1	0	110
08:15	0	36	21	0	11	18	0	0	3	17	7	0	7	6	3	0	129
*** BREAK ***																	
Total	0	74	34	0	20	33	0	0	4	29	13	0	16	12	4	0	239
*** BREAK ***												,					
16:00	0	21	9	0	6	8	1	0	1	20	9	0	20	8	0	0	103
16:15	0	10	6	0	2	4	2	0	1	31	9	0	13	16	1	0	95
16:30	2	21	2	0	7	3	0	0	1	28	8	0	17	15	2	0	106
16:45	1	18	8	0	1	3	1	0	3	25	7	0	14	9	0	0	90
Total	3	70	25	0	16	18	4	0	6	104	33	0	64	48	3	0	394
17:00	1	19	11	0	3	4	4	0	1	30	9	0	19	8	2	0	111
17:15	0	9	6	0	2	3	0	0	0	23	10	0	25	14	2	0	94
17:30	0	20	6	0	7	7	0	0	0	21	13	0	16	20	5	0	115
17:45	0	14	5	0	9	4	0	0	0	34	5	0	14	16	1	0	102
Total	1	62	28	0	21	18	4	0	1	108	37	0	74	58	10	0	422
Grand Total	9	421	220	0	127	165	11	0	21	334	99	0	213	144	32	0	1796
Apprch %	1.4	64.8	33.8	0	41.9	54.5	3.6	0	4.6	73.6	21.8	0	54.8	37	8.2	0	
Total %	0.5	23.4	12.2	0	7.1	9.2	0.6	0	1.2	18.6	5.5	0	11.9	8	1.8	0	
Unshifted	7	401	176	0	119	146	10	0	18	325	88	0	159	133	31	0	1613
% Unshifted	77.8	95.2	80	0	93.7	88.5	90.9	0	85.7	97.3	88.9	0	74.6	92.4	96.9	0	89.8
Bank 1	1	19	42	0	8	18	1	0	3	9	11	0	52	11	1	0	176
% Bank 1	11.1	4.5	19.1	0	6.3	10.9	9.1	0	14.3	2.7	11.1	0	24.4	7.6	3.1	0	9.8
Bank 2	1	1	2	0	0	1	0	0	0	0	0	0	2	0	0	0	7

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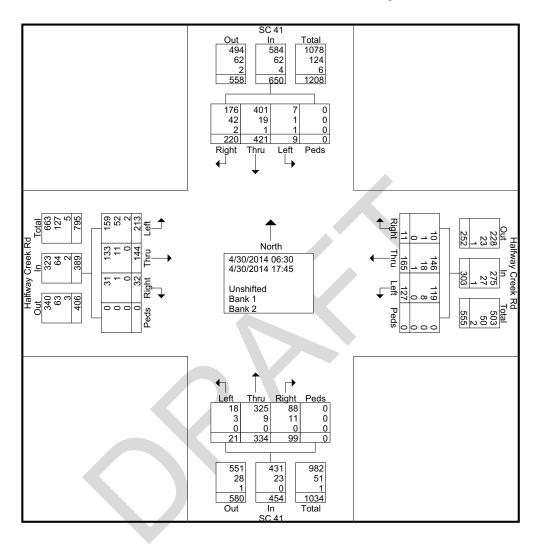
Select File/Preference in the Main Scree

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**Default Comments** 

File Name: SC 41 @ Halfway Creek Rd

Site Code : 00043014 Start Date : 4/30/2014



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**Default Comments** 

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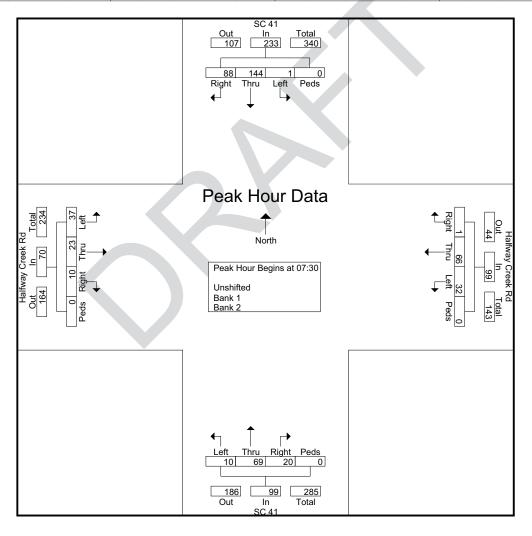
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Then Click the Comments Tab

File Name: SC 41 @ Halfway Creek Rd

Site Code : 00043014 Start Date : 4/30/2014

			SC 41				Halfv	vay Cre	ek Rd				SC 41				Halfv	vay Cre	ek Rd		]
		So	uthbou	nd			W	estbou	nd			N	orthbou	ınd			E	astbour	nd		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour An	alysis F	rom 06:	:30 to 0	8:15 - I	Peak 1 of	1															
Peak Hour for	Entire I	ntersec	tion Be	gins at	07:30																
07:30	1	35	31	0	67	6	20	1	0	27	6	18	5	0	29	8	6	4	0	18	141
07:45	0	35	23	0	58	6	13	0	0	19	0	22	2	0	24	13	5	2	0	20	121
08:00	0	38	13	0	51	9	15	0	0	24	1	12	6	0	19	9	6	1	0	16	110
08:15	0	36	21	0	57	11	18	0	0	29	3	17	7	0	27	7	6	3	0	16	129
Total Volume	1	144	88	0	233	32	66	1	0	99	10	69	20	0	99	37	23	10	0	70	501
% App. Total	0.4	61.8	37.8	0		32.3	66.7	1	0		10.1	69.7	20.2	0		52.9	32.9	14.3	0		
PHF	.250	.947	.710	.000	.869	.727	.825	.250	.000	.853	.417	.784	.714	.000	.853	.712	.958	.625	.000	.875	.888



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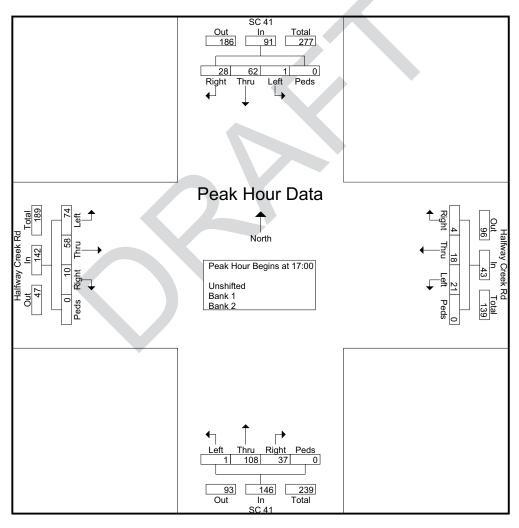
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Then Click the Comments Tab

File Name: SC 41 @ Halfway Creek Rd

Site Code : 00043014 Start Date : 4/30/2014

		· ·	SC 41	,				ay Cre				N	SC 41					vay Cre			
		So	<u>uthbou</u>	nd			W	estbou	na			N	<u>orthbou</u>	ınd			E	astbour	าต		
Start Time	Left	Thr u	Rig ht	Ped s	App. Total	Left	Thr u	Rig ht	Ped s	App. Total	Left	Thr u	Right	Peds	App. Total	Left	Thr u	Right	Peds	App. Total	Int. Total
Peak Hour Ana	alysis F	rom 16:	00 to 1	7:45 - I	Peak 1 of	1															
Peak Hour for	Entire I	ntersect	tion Be	gins at	17:00																
17:00	1	19	11	0	31	3	4	4	0	11	1	30	9	0	40	19	8	2	0	29	111
17:15	0	9	6	0	15	2	3	0	0	5	0	23	10	0	33	25	14	2	0	41	94
17:30	0	20	6	0	26	7	7	0	0	14	0	21	13	0	34	16	20	5	0	41	115
17:45	0	14	5	0	19	9	4	0	0	13	0	34	5	0	39	14	16	1	0	31	102
Total Volume	1	62	28	0	91	21	18	4	0	43	1	108	37	0	146	74	58	10	0	142	422
% App. Total	1.1	68.1	30.8	0		48.8	41.9	9.3	0		0.7	74	25.3	0		52.1	40.8	. 7	0		
PHF	.250	.775	.636	.000	.734	.583	.643	.250	.000	.768	.250	.794	.712	.000	.913	.740	.725	.500	.000	.866	.917



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File Name: SC 41 @ Clements Ferry Rd

Site Code : 00043014 Start Date : 4/30/2014

					(	Groups P	rinted- U	nshifted	- Bank 1	- Bank 2							
		SC -				Westb			Duin 1	SC Northb	41		Cl	ements I	Ferry Rd		
Start Time	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Int. Total
06:30	0	57	0	0	0	0	0	0	144	8	0	0	0	0	51	0	260
06:45	0	54	0	0	0	0	0	0	124	11	0	0	0	0	60	0	249
Total	0	111	0	0	0	0	0	0	268	19	0	0	0	0	111	0	509
07:00	0	48	0	0	0	0	0	0	150	21	0	0	0	0	92	0	311
07:15	0	51	0	0	0	0	0	0	137	27	0	0	0	0	83	0	298
07:30	0	54	0	0	0	0	0	0	122	21	0	0	1	0	103	0	301
07:45	0	46	0	0	0	0	0	0	126	26	0	0	1	0	92	0	291
Total	0	199	0	0	0	0	0	0	535	95	0	0	2	0	370	0	1201
08:00	0	45	0	0	0	0	0	0	114	20	0	0	0	0	91	0	270
08:15	0	54	0	0	0	0	0	0	120	22	0	0	0	0	79	0	275
*** BREAK ***																	
Total	0	99	0	0	0	0	0	0	234	42	0	0	0	0	170	0	545
*** BREAK ***																	
16:00	0	32	0	0	0	0	0	0	60	36	0	1	0	0	111	0	240
16:15	0	14	0	0	0	0	0	0	89	39	0	0	0	0	106	0	248
16:30	0	26	0	0	0	0	0	0	76	41	0	0	0	0	135	0	278
16:45	0	25	0	0	0	0	0	0	68	41	0	0	0	0	150	0	284
Total	0	97	0	0	0	0	0	0	293	157	0	1	0	0	502	0	1050
17:00	0	27	1	0	0	0	0	0	65	42	0	0	0	0	157	0	292
17:15	0	12	0	0	0	0	0	0	78	36	0	0	0	0	195	0	321
17:30	0	28	0	0	0	0	0	0	80	39	0	0	0	0	196	0	343
17:45	0	29	0	0	0	0	0	0	72	44	0	0	0	0	169	0	314
Total	0	96	1	0	0	0	0	0	295	161	0	0	0	0	717	0	1270
Grand Total	0	602	1	0	0	0	0	0	1625	474	0	1	2	0	1870	0	4575
Apprch %	0	99.8	0.2	0	0	0	0	0	77.4	22.6	0	0	0.1	0	99.9	0	
Total %	0	13.2	0	0	0	0	0	0	35.5	10.4	0	0	00	0	40.9	0	
Unshifted	0	568	1	0	0	0	0	0	1606	450	0	1	2	0	1836	0	4464
% Unshifted	0	94.4	100	0	0	0	0	0	98.8	94.9	0	100	100	0	98.2	0	97.6
Bank 1	0	33	0	0	0	0	0	0	18	24	0	0	0	0	30	0	105
% Bank 1	0	5.5	0	0	0	0	0	0	1.1	5.1	0_	0	0	0	1.6	0	2.3

735 Maryland St. Columbia, SC 29201

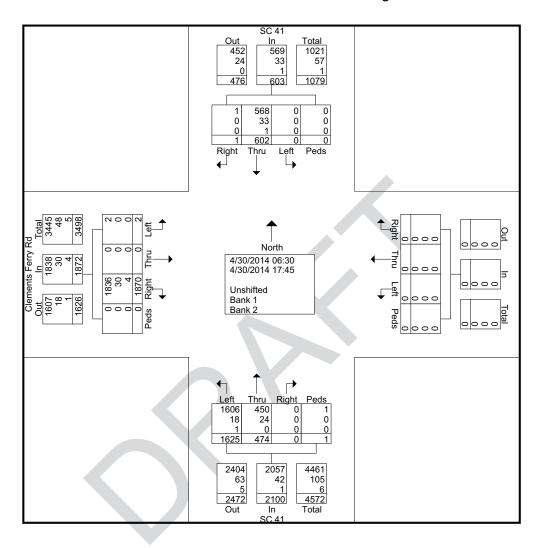
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**Default Comments** 

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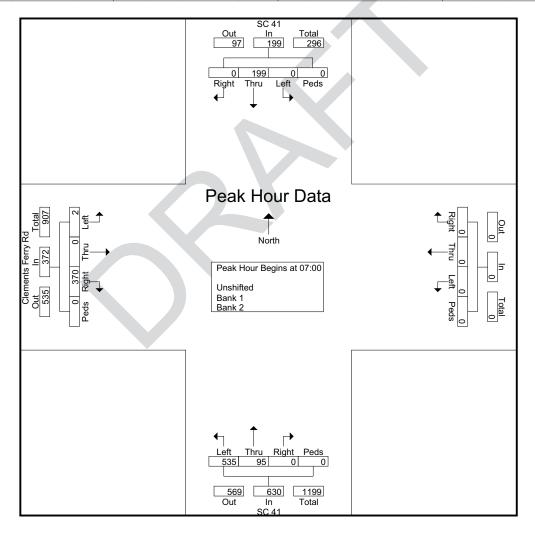
Change These in The Preferences Window Select File/Preference in the Main Scree

Then Click the Comments Tab

File Name: SC 41 @ Clements Ferry Rd

Site Code : 00043014 Start Date : 4/30/2014

			SC 41										SC 41				Cleme	ents Fe	rry Rd		]
		So	uthbou	nd			W	estbou	nd			N	orthbou	ınd			E	astbou	nd		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour An	alysis F	rom 06:	30 to 0	8:15 - I	Peak 1 of	1															
Peak Hour for	Entire I	ntersec	tion Be	gins at	07:00																
07:00	0	48	0	0	48	0	0	0	0	0	150	21	0	0	171	0	0	92	0	92	311
07:15	0	51	0	0	51	0	0	0	0	0	137	27	0	0	164	0	0	83	0	83	298
07:30	0	54	0	0	54	0	0	0	0	0	122	21	0	0	143	1	0	103	0	104	301
07:45	0	46	0	0	46	0	0	0	0	0	126	26	0	0	152	1	0	92	0	93	291
Total Volume	0	199	0	0	199	0	0	0	0	0	535	95	0	0	630	2	0	370	0	372	1201
% App. Total	0	100	0	0		0	0	0	0		84.9	15.1	0	0		0.5	0	99.5	0		
PHF	.000	.921	.000	.000	.921	.000	.000	.000	.000	.000	.892	.880	.000	.000	.921	.500	.000	.898	.000	.894	.965



735 Maryland St. Columbia, SC 29201

**Default Comments** 

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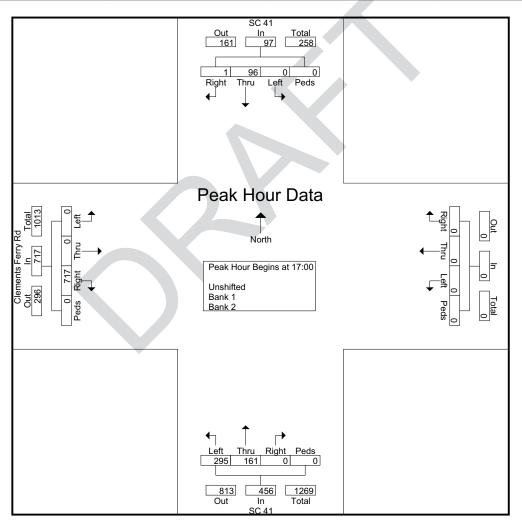
Change These in The Preferences Window Select File/Preference in the Main Scree

Then Click the Comments Tab

File Name: SC 41 @ Clements Ferry Rd

Site Code : 00043014 Start Date : 4/30/2014

			SC 41										SC 41					ents Fe	-		]
		So	uthbou	nd			W	estbou	nd			N	<u>orthbou</u>	ınd			E	astbou	nd		
Start Time	Left	Thr u	Rig ht	Ped s	App. Total	Left	Thr u	Rig ht	Ped s	App. Total	Left	Thr u	Right	Peds	App. Total	Left	Thr u	Right	Peds	App. Total	Int. Total
Peak Hour Ana	alysis Fi	rom 16:	00 to 1'	7:45 - F	Peak 1 of	1															
Peak Hour for	Entire I	ntersect	tion Beg	gins at	17:00																
17:00	0	27	1	0	28	0	0	0	0	0	65	42	0	0	107	0	0	157	0	157	292
17:15	0	12	0	0	12	0	0	0	0	0	78	36	0	0	114	0	0	195	0	195	321
17:30	0	28	0	0	28	0	0	0	0	0	80	39	0	0	119	0	0	196	0	196	343
17:45	0	29	0	0	29	0	0	0	0	0	72	44	0	0	116	0	0	169	0	169	314
Total Volume	0	96	1	0	97	0	0	0	0	0	295	161	0	0	456	0	0	717	0	717	1270
% App. Total	0	99	1	0		0	0	0	0		64.7	35.3	0	0		0	0	100	0		
PHF	.000	.828	.250	.000	.836	.000	.000	.000	.000	.000	.922	.915	.000	.000	.958	.000	.000	.915	.000	.915	.926



### 735 Maryland St. Columbia, SC 29201

**Default Comments** 

You Can Count On File Name: Clements Ferry @ Reflectance Dr Site Code: 00043014

Change These in The Preferences Window Select File/Preference in the Main Scree

Start Date : 4/30/2014

Then Click the Comments Tab

					(	Groups P	rinted- U	nshifted	- Bank 1	- Bank 2							
	]	Reflecta	nce Dr			Clement				Cainhoy 1				Clement	s Ferry		
		Southb	ound			Westb	ound			North	ound			Eastb	ound		
Start Time	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Left	Thru	Right	Peds	Int. Total
06:30	0	0	45	0	0	138	0	0	0	0	0	0	20	42	0	1	246
06:45	2	0	40	0	0	133	1_	0	0	0	3_	0	10	62	0	0	251
Total	2	0	85	0	0	271	1	0	0	0	3	0	30	104	0	1	497
07:00	0	0	28	0	0	148	0	0	2	0	1	0	12	90	0	0	281
07:15	1	0	34	0	1	140	0	0	1	0	1	0	16	80	0	0	274
07:30	0	0	53	0	1	127	0	0	1	0	3	0	15	97	0	0	297
07:45	1	0	40	0	0	121	1	0	1	0	1	0	21	91	0	0	277
Total	2	0	155	0	2	536	1	0	5	0	6	0	64	358	0	0	1129
08:00	0	0	34	0	0	120	0	0	0	0	1	0	15	89	0	0	259
08:15	0	0	46	0	0	117	0	0	2	0	2	0	8	81	0	0	256
*** BREAK ***																	
Total	0	0	80	0	0	237	0	0	2	0	3	0	23	170	0	0	515
*** BREAK ***												•					
16:00	1	0	18	0	0	63	0	0	1	0	0	0	27	120	2	0	232
16:15	1	0	11	0	1	77	0	0	0	0	0	0	35	116	1	0	242
16:30	0	0	6	0	0	72	0	0	1	0	0	0	28	138	1	0	246
16:45	0	0	14	0	0	69	0	0	0	0	2	0	27	153	1	0	266
Total	2	0	49	0	1	281	0	0	2	0	2	0	117	527	5	0	986
17:00	0	0	17	0	1	65	0	0	1	0	1	0	41	178	4	0	308
17:15	0	0	11	0	0	77	1	0	1	0	0	0	45	188	1	0	324
17:30	0	0	14	0	3	70	2	0	1	0	1	0	38	185	2	0	316
17:45	0	0	11	0	0	77	0	0	2	0	1	0	28	170	1	0	290
Total	0	0	53	0	4	289	3	0	5	0	3	0	152	721	8	0	1238
Grand Total	6	0	422	0	7	1614	5	0	14	0	17	0	386	1880	13	1	4365
Apprch %	1.4	0	98.6	0	0.4	99.3	0.3	0	45.2	0	54.8	0	16.9	82.5	0.6	0	
Total %	0.1	0	9.7	0	0.2	37	0.1	0	0.3	0	0.4	0	8.8	43.1	0.3	0	
Unshifted	6	0	357	0	7	1600	5	0	14	0	17	0	322	1848	13	1	4190
% Unshifted	100	00	84.6	0	100	99.1	100	0	100	0	100	0	83.4	98.3	100	100	96
Bank 1	0	0	62	0	0	13	0	0	0	0	0	0	62	27	0	0	164
% Bank 1	0	0_	14.7	0	0	0.8	0	0	0	0	0_	0	16.1	1.4	0_	0	3.8
Bank 2	0	0	3	0	0	1	0	0	0	0	0	0	2	5	0	0	11
% Bank 2	0	0	0.7	0	0	0.1	0	0	0	0	0	0	0.5	0.3	0	0	0.3

735 Maryland St. Columbia, SC 29201

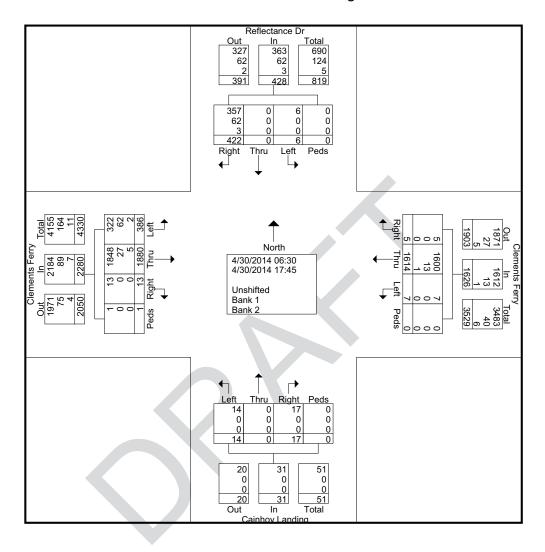
**Default Comments** 

You Can Count On File Name : Clements Ferry @ Reflectance Dr

Change These in The Preferences Window Select File/Preference in the Main Scree

Site Code : 00043014 Start Date : 4/30/2014

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735 Maryland St. Columbia, SC 29201

**Default Comments** 

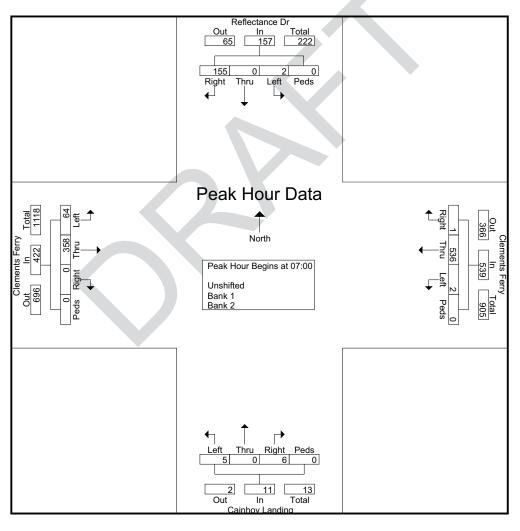
You Can Count On File Name : Clements Ferry @ Reflectance Dr

Change These in The Preferences Window Select File/Preference in the Main Scree

Site Code : 00043014 Start Date : 4/30/2014

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			lectance					ments F	-				hoy La	-				ments F	-		]
		So	uthbou	ınd			W	/estbou	nd			N	<u>orthbou</u>	ınd			E	astbour	ıd		
Start Time	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Left	Thru	Right	Peds	App. Total	Int. Total
Peak Hour Ana	alysis F	rom 06	:30 to 0	8:15 - I	Peak 1 of	1															
Peak Hour for	Entire I	ntersec	tion Be	gins at	07:00																
07:00	0	0	28	0	28	0	148	0	0	148	2	0	1	0	3	12	90	0	0	102	281
07:15	1	0	34	0	35	1	140	0	0	141	1	0	1	0	2	16	80	0	0	96	274
07:30	0	0	53	0	53	1	127	0	0	128	1	0	3	0	4	15	97	0	0	112	297
07:45	1	0	40	0	41	0	121	1	0	122	1	0	1	0	2	21	91	0	0	112	277
Total Volume	2	0	155	0	157	2	536	1	0	539	5	0	6	0	11	64	358	0	0	422	1129
% App. Total	1.3	0	98.7	0		0.4	99.4	0.2	0		45.5	0	54.5	0		15.2	84.8	0	0		
PHF	.500	.000	.731	.000	.741	.500	.905	.250	.000	.910	.625	.000	.500	.000	.688	.762	.923	.000	.000	.942	.950



735 Maryland St. Columbia, SC 29201

**Default Comments** 

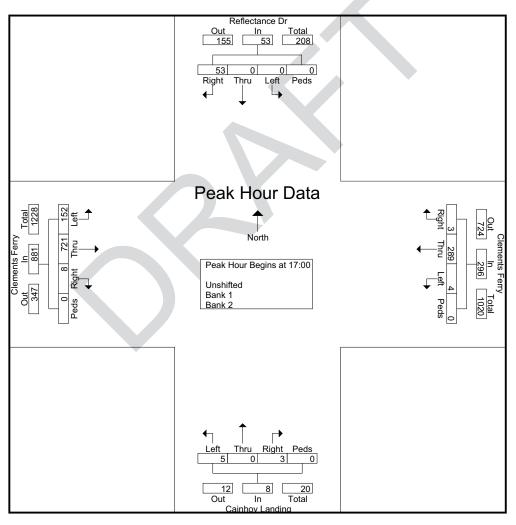
You Can Count On File Name : Clements Ferry @ Reflectance Dr

Change These in The Preferences Window Select File/Preference in the Main Scree

Site Code : 00043014 Start Date : 4/30/2014

Then Click the Comments Tab

			ectance uthbou					nents F	•				hoy La	$\mathcal{L}$				ments F	-		
Start Time	Left	Thr u	Rig ht	Ped s	App. Total	Left	Thr u	Rig ht	Ped s	App. Total	Left	Thr u	Right	Peds	App. Total	Left	Thr u	Right	Peds	App. Total	Int. Total
Peak Hour An	alysis F	rom 16:	00 to 1	7:45 - I	Peak 1 of	1										•				•	
Peak Hour for	Entire I	ntersec	tion Be	gins at	17:00																
17:00	0	0	17	0	17	1	65	0	0	66	1	0	1	0	2	41	178	4	0	223	308
17:15	0	0	11	0	11	0	77	1	0	78	1	0	0	0	1	45	188	1	0	234	324
17:30	0	0	14	0	14	3	70	2	0	75	1	0	1	0	2	38	185	2	0	225	316
17:45	0	0	11	0	11	0	77	0	0	77	2	0	1	0	3	28	170	1	0	199	290
Total Volume	0	0	53	0	53	4	289	3	0	296	5	0	3	0	8	152	721	8	0	881	1238
% App. Total	0	0	100	0		1.4	97.6	1	0		62.5	0	37.5	0		17.3	81.8	0.9	0		
PHF	.000	.000	.779	.000	.779	.333	.938	.375	.000	.949	.625	.000	.750	.000	.667	.844	.959	.500	.000	.941	.955



# APPENDIX B Existing Conditions

	_⊀	<b>→</b>	+	٤	6	1	
Movement	EBL	EBT	WBT	WBR	SWL	SWR	
Lane Configurations		ર્ન	ĵ»		W		
Volume (veh/h)	64	358	536	1	2	155	
Sign Control		Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.76	0.92	0.91	0.90	0.50	0.73	
Hourly flow rate (vph)	84	389	589	1	4	212	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type		None	None				
Median storage veh)							
Upstream signal (ft)							
pX, platoon unblocked							
vC, conflicting volume	590				1147	590	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	590				1147	590	
tC, single (s)	4.1				6.4	6.2	
tC, 2 stage (s)							
tF (s)	2.2				3.5	3.3	
p0 queue free %	91				98	58	
cM capacity (veh/h)	985				201	508	
Direction, Lane #	EB 1	WB 1	SW 1				
Volume Total	473	590	216				
Volume Left	84	0	4		7		
Volume Right	0	1	212				
cSH	985	1700	494				
Volume to Capacity	0.09	0.35	0.44				
Queue Length 95th (ft)	7	0	55				
Control Delay (s)	2.4	0.0	17.8				
Lane LOS	A		С				
Approach Delay (s)	2.4	0.0	17.8				
Approach LOS			С				
Intersection Summary							
Average Delay			3.9				
Intersection Capacity Utili	ization		70.4%	IC	U Level	of Service	
Analysis Period (min)			15				

	*	<b>†</b>	7	¥	<b>↓</b>	لِر	Ť	×	4	4	×	t
Movement	NBL	NBT	NBR	SBL	SBT	SBR	NEL	NET	NER	SWL	SWT	SWR
Lane Configurations		4			4			44			4	
Volume (veh/h)	3	131	91	7	76	13	37	17	12	39	61	3
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.75	0.94	0.73	0.29	0.86	0.65	0.71	0.71	0.60	0.70	0.76	0.75
Hourly flow rate (vph)	4	139	125	24	88	20	52	24	20	56	80	4
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)												
pX, platoon unblocked												
vC, conflicting volume	108			264			400	419	98	388	366	202
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	108			264			400	419	98	388	366	202
tC, single (s)	4.1			4.1			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	100			98		Y	89	95	98	89	85	100
cM capacity (veh/h)	1482			1300			487	514	958	530	550	839
Direction, Lane #	NB 1	SB 1	NE 1	SW 1								
Volume Total	268	133	96	140								
Volume Left	4	24	52	56								
Volume Right	125	20	20	4								
cSH	1482	1300	551	547								
Volume to Capacity	0.00	0.02	0.17	0.26								
Queue Length 95th (ft)	0	1	16	25								
Control Delay (s)	0.1	1.6	12.9	13.8								
Lane LOS	Α	A	В	В								
Approach Delay (s)	0.1	1.6	12.9	13.8								
Approach LOS			В	В								
Intersection Summary												
Average Delay			5.4									
Intersection Capacity Utiliza	ation		26.0%	IC	CU Level	of Service			Α			
Analysis Period (min)			15									

	•	•	<b>†</b>	<i>&gt;</i>	<b>\</b>	ţ		
Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	7	7	<b>†</b>	7	J.	<b>†</b>		
Volume (veh/h)	199	0	535	95	0	370		
Sign Control	Stop		Free			Free		
Grade	0%		0%			0%		
Peak Hour Factor	0.92	0.90	0.89	0.88	0.90	0.90		
Hourly flow rate (vph)	216	0	601	108	0	411		
Pedestrians								
Lane Width (ft)								
Walking Speed (ft/s)								
Percent Blockage								
Right turn flare (veh)		8						
Median type			TWLTL			None		
Median storage veh)			2					
Upstream signal (ft)								
pX, platoon unblocked								
vC, conflicting volume	1012	601			601			
vC1, stage 1 conf vol	601							
vC2, stage 2 conf vol	411							
vCu, unblocked vol	1012	601			601			
tC, single (s)	6.4	6.2			4.1			
tC, 2 stage (s)	5.4	V. <u>_</u>						
tF (s)	3.5	3.3			2.2			
p0 queue free %	54	100			100			
cM capacity (veh/h)	473	500			976			
· · · · · · · · · · · · · · · · · · ·			NID 0	00.4				
Direction, Lane #	WB 1	NB 1	NB 2	SB 1	SB 2			
Volume Total	216	601	108	0	411			
Volume Left	216	0	0	0	0			
Volume Right	0	0	108	0	0			
cSH	467	1700	1700	1700	1700			
Volume to Capacity	0.46	0.35	0.06	0.00	0.24			
Queue Length 95th (ft)	60	0	0	0	0			
Control Delay (s)	19.2	0.0	0.0	0.0	0.0			
Lane LOS	С							
Approach Delay (s)	19.2	0.0		0.0				
Approach LOS	С	~						
Intersection Summary								
Average Delay			3.1					
Intersection Capacity Utiliz	ation		45.8%	IC	U Level	Service	Α	
Analysis Period (min)			15					

	_#	-	<b>←</b>	۲	6	✓	
Movement	EBL	EBT	WBT	WBR	SWL	SWR	
Lane Configurations		ર્ન	<b>^</b>		W		
Volume (veh/h)	152	721	289	3	0	53	
Sign Control		Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.84	0.96	0.94	0.38	0.50	0.78	
Hourly flow rate (vph)	181	751	307	8	0	68	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type		None	None				
Median storage veh)							
Upstream signal (ft)							
pX, platoon unblocked							
vC, conflicting volume	315				1424	311	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	315				1424	311	
tC, single (s)	4.1				6.4	6.2	
tC, 2 stage (s)							
tF (s)	2.2				3.5	3.3	
p0 queue free %	85				100	91	
cM capacity (veh/h)	1245				128	729	
Direction, Lane #	EB 1	WB 1	SW 1				
Volume Total	932	315	68				
Volume Left	181	0	0				
Volume Right	0	8	68				
cSH	1245	1700	729				
Volume to Capacity	0.15	0.19	0.09				
Queue Length 95th (ft)	13	0	8				
Control Delay (s)	3.4	0.0	10.4				
Lane LOS	Α		В				
Approach Delay (s)	3.4	0.0	10.4				
Approach LOS			В				
Intersection Summary							
Average Delay			2.9				
Intersection Capacity Utiliza	ation		75.1%	IC	U Level	of Service	
Analysis Period (min)			15				
. , ,							

	*	<b>†</b>	7	<b>₩</b>	ļ	لِ	Ť	×	4	4	×	t
Movement	NBL	NBT	NBR	SBL	SBT	SBR	NEL	NET	NER	SWL	SWT	SWR
Lane Configurations		4			44			44			4	
Volume (veh/h)	1	108	37	1	62	28	74	58	10	21	18	4
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.25	0.79	0.71	0.25	0.78	0.64	0.74	0.73	0.50	0.58	0.64	0.25
Hourly flow rate (vph)	4	137	52	4	79	44	100	79	20	36	28	16
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)												
pX, platoon unblocked												
vC, conflicting volume	123			189			310	306	101	340	302	163
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	123			189			310	306	101	340	302	163
tC, single (s)	4.1			4.1			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	100			100		Y	83	87	98	93	95	98
cM capacity (veh/h)	1464			1385			606	604	954	538	607	882
Direction, Lane #	NB 1	SB 1	NE 1	SW 1								
Volume Total	193	127	199	80								
Volume Left	4	4	100	36								
Volume Right	52	44	20	16								
cSH	1464	1385	628	610								
Volume to Capacity	0.00	0.00	0.32	0.13								
Queue Length 95th (ft)	0	0	34	11								
Control Delay (s)	0.2	0.3	13.4	11.8								
Lane LOS	А	A	В	В								
Approach Delay (s)	0.2	0.3	13.4	11.8								
Approach LOS			В	В								
Intersection Summary												
Average Delay			6.1									
Intersection Capacity Utiliza	ation		25.2%	IC	CU Level	of Service			Α			
Analysis Period (min)			15									
,												

•	•	<b>†</b>	<b>/</b>	<b>&gt;</b>	<b>↓</b>	
WBL	WBR	NBT	NBR	SBL	SBT	
Ĭ	7	<b>^</b>	7	, N	<b>†</b>	
96	0	295	161	0	717	
Stop		Free			Free	
0%		0%			0%	
0.83	0.90	0.92	0.91	0.90	0.91	
116	0	321	177	0	788	
	8					
		TWLTL			None	
		2				
1109	321			321		
	321			321		
6.4	6.2			4.1		
5.4						
3.5	3.3			2.2		
72	100					
413	720			1239		
WB 1	NB 1	NB 2	SB 1	SB 2		
	3.0	3.0	0.0	3.0		
	0.0		0.0			
C	0.0		0.0			
		1 Δ				
ation			IC	اااويوا	of Service	Α
ation i			10	O LGVOI	OI OOI VIOC	Λ
		10				
	96 Stop 0% 0.83 116 1109 321 788 1109 6.4 5.4 3.5 72 413 WB 1 116 116 0 403 0.29 29 17.5 C	96 0 Stop 0% 0.83 0.90 116 0 8 1109 321 788 1109 321 6.4 6.2 5.4 3.5 3.3 72 100 413 720 WB 1 NB 1 116 321 116 0 0 0 403 1700 0.29 0.19 29 0 17.5 0.0 C	96 0 295 Stop Free 0% 0% 0.83 0.90 0.92 116 0 321  8 TWLTL 2  1109 321 321 788 1109 321 6.4 6.2 5.4 3.5 3.3 72 100 413 720  WB 1 NB 1 NB 2 116 321 177 116 0 0 0 0 177 403 1700 1700 0.29 0.19 0.10 29 0 0 17.5 0.0 0.0 C 17.5 0.0 0.0 C	96  0  295  161  Stop	96  0  295  161  0	96  0  295  161  0  717  Stop

### APPENDIX C 2021 "No-Build" Traffic Conditions

	•	•	<b>†</b>	~	<b>\</b>	<b>+</b>		
Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	*	7	<b>*</b>	7	7	<b>†</b>		
Volume (vph)	213	0	574	102	0	397		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Total Lost time (s)	6.0		6.0	6.0		6.0		
Lane Util. Factor	1.00		1.00	1.00		1.00		
Frt	1.00		1.00	0.85		1.00		
Flt Protected	0.95		1.00	1.00		1.00		
Satd. Flow (prot)	1770		1863	1583		1863		
Flt Permitted	0.95		1.00	1.00		1.00		
Satd. Flow (perm)	1770		1863	1583		1863		
Peak-hour factor, PHF	0.92	0.90	0.89	0.88	0.90	0.90		
Adj. Flow (vph)	232	0	645	116	0	441		
RTOR Reduction (vph)	0	0	0	54	0	0		
Lane Group Flow (vph)	232	0	645	62	0	441		
Turn Type	Perm	Perm	NA	Perm	pm+pt	NA		
Protected Phases			6		5	2		
Permitted Phases	4	4		6	2			
Actuated Green, G (s)	11.9		27.7	27.7		27.7		
Effective Green, g (s)	11.9		27.7	27.7		27.7		
Actuated g/C Ratio	0.23		0.54	0.54		0.54		
Clearance Time (s)	6.0		6.0	6.0		6.0		
Vehicle Extension (s)	3.0		3.0	3.0		3.0		
Lane Grp Cap (vph)	408		1000	849		1000		
v/s Ratio Prot			c0.35			0.24		
v/s Ratio Perm	c0.13			0.04				
v/c Ratio	0.57		0.65	0.07		0.44		
Uniform Delay, d1	17.6		8.5	5.8		7.3		
Progression Factor	1.00		1.00	1.00		1.00		
Incremental Delay, d2	1.8		1.4	0.0		0.3		
Delay (s)	19.4		9.9	5.8		7.6		
Level of Service	В		Α	Α		Α		
Approach Delay (s)	19.4		9.3			7.6		
Approach LOS	В		Α			Α		
Intersection Summary								
HCM 2000 Control Delay			10.4	F	ICM 2000	Level of S	ervice B	
HCM 2000 Volume to Capa	city ratio		0.73					
Actuated Cycle Length (s)			51.6	S	Sum of lost	t time (s)	18.0	
Intersection Capacity Utiliza	ation		52.0%	10	CU Level	of Service	Α	
Analysis Period (min)			15					
c Critical Lane Group								

	_#	<b>→</b>	+	٤	4	✓	
Movement	EBL	EBT	WBT	WBR	SWL	SWR	
Lane Configurations		ર્ન	<b>^</b>		W		
Volume (veh/h)	69	384	575	1	2	166	
Sign Control		Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.76	0.92	0.91	0.90	0.50	0.73	
Hourly flow rate (vph)	91	417	632	1	4	227	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type		None	None				
Median storage veh)							
Upstream signal (ft)							
pX, platoon unblocked							
vC, conflicting volume	633				1231	632	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	633				1231	632	
tC, single (s)	4.1				6.4	6.2	
tC, 2 stage (s)							
tF (s)	2.2				3.5	3.3	
p0 queue free %	90				98	53	
cM capacity (veh/h)	950				177	480	
Direction, Lane #	EB 1	WB 1	SW 1				
Volume Total	508						
Volume Left	91	633	231				
		0	227				
Volume Right	0	1700	227				
cSH	950	1700	466				
Volume to Capacity	0.10	0.37	0.50				
Queue Length 95th (ft)	8	0	68				
Control Delay (s)	2.6	0.0	20.1				
Lane LOS	A	0.0	C 20.4				
Approach Delay (s)	2.6	0.0	20.1				
Approach LOS			С				
Intersection Summary							
Average Delay			4.3				
Intersection Capacity Utiliz	zation		74.7%	IC	CU Level	of Service	
Analysis Period (min)			15				

	*1	<b>†</b>	7	(#	<b>↓</b>	لِر	Ť	×	4	€	×	t
Movement	NBL	NBT	NBR	SBL	SBT	SBR	NEL	NET	NER	SWL	SWT	SWR
Lane Configurations		4			4			4			4	
Volume (veh/h)	1	116	40	1	66	30	79	62	11	23	19	4
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Hourly flow rate (vph)	1	129	44	1	73	33	88	69	12	26	21	4
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)												
pX, platoon unblocked												
vC, conflicting volume	107			173			261	268	90	292	262	151
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	107			173			261	268	90	292	262	151
tC, single (s)	4.1			4.1			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	100			100			87	89	99	96	97	100
cM capacity (veh/h)	1484			1403			671	637	968	597	642	895
Direction, Lane #	NB 1	SB 1	NE 1	SW 1								
Volume Total	174	108	169	51								
Volume Left	1	1	88	26								
Volume Right	44	33	12	4								
cSH	1484	1403	671	634								
Volume to Capacity	0.00	0.00	0.25	0.08								
Queue Length 95th (ft)	0	0	25	7								
Control Delay (s)	0.1	0.1	12.2	11.2								
Lane LOS	Α	A	В	В								
Approach Delay (s)	0.1	0.1	12.2	11.2								
Approach LOS			В	В								
Intersection Summary												
Average Delay			5.3									
Intersection Capacity Utiliz	ation		26.4%	IC	CU Level	of Service			Α			
Analysis Period (min)			15									
· ,												

	•	•	<b>†</b>	<b>/</b>	<b>\</b>	ļ			
Movement	WBL	WBR	NBT	NBR	SBL	SBT			
Lane Configurations	ሻ	7	<b>†</b>	7	Ť	<b>†</b>			
Volume (vph)	103	0	316	173	0	769			
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900			
Total Lost time (s)	6.0		6.0	6.0		6.0			
Lane Util. Factor	1.00		1.00	1.00		1.00			
Frt	1.00		1.00	0.85		1.00			
Flt Protected	0.95		1.00	1.00		1.00			
Satd. Flow (prot)	1770		1863	1583		1863			
Flt Permitted	0.95		1.00	1.00		1.00			
Satd. Flow (perm)	1770		1863	1583		1863			
Peak-hour factor, PHF	0.90	0.90	0.90	0.90	0.90	0.90			
Adj. Flow (vph)	114	0	351	192	0	854			
RTOR Reduction (vph)	0	0	0	66	0	0			
Lane Group Flow (vph)	114	0	351	126	0	854			
Turn Type	Perm	Perm	NA	Perm	pm+pt	NA			
Protected Phases			6		5	2			
Permitted Phases	4	4		6	2				
Actuated Green, G (s)	7.4		37.2	37.2		37.2			
Effective Green, g (s)	7.4		37.2	37.2		37.2			
Actuated g/C Ratio	0.13		0.66	0.66		0.66			
Clearance Time (s)	6.0		6.0	6.0		6.0			
Vehicle Extension (s)	3.0		3.0	3.0		3.0			
Lane Grp Cap (vph)	231		1224	1040		1224			
v/s Ratio Prot			0.19			c0.46			
v/s Ratio Perm	c0.06			0.08					
v/c Ratio	0.49		0.29	0.12		0.70			
Uniform Delay, d1	22.9		4.1	3.6		6.1			
Progression Factor	1.00		1.00	1.00		1.00			
Incremental Delay, d2	1.7		0.1	0.1		1.8			
Delay (s)	24.5		4.2	3.7		7.9			
Level of Service	С		Α	Α		Α			
Approach Delay (s)	24.5		4.0			7.9			
Approach LOS	С		Α			Α			
Intersection Summary			·						
HCM 2000 Control Delay			7.8	Н	ICM 2000	Level of Se	ervice	Α	 
HCM 2000 Volume to Capa	city ratio		0.77						
Actuated Cycle Length (s)	-		56.6	S	um of lost	t time (s)		18.0	
Intersection Capacity Utiliza	ation		56.2%			of Service		В	
Analysis Period (min)			15						
c Critical Lane Group									

	_#	<b>→</b>	+	٤	4	1	
Movement	EBL	EBT	WBT	WBR	SWL	SWR	
Lane Configurations		ર્ન	ĵ,		W		
Volume (veh/h)	163	773	310	3	0	57	
Sign Control		Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	
Hourly flow rate (vph)	181	859	344	3	0	63	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type		None	None				
Median storage veh)							
Upstream signal (ft)							
oX, platoon unblocked							
vC, conflicting volume	348				1567	346	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	348				1567	346	
tC, single (s)	4.1				6.4	6.2	
tC, 2 stage (s)							
tF (s)	2.2				3.5	3.3	
p0 queue free %	85				100	91	
cM capacity (veh/h)	1211				104	697	
Direction, Lane #	EB 1	WB 1	SW 1				
Volume Total	1040	348	63				
Volume Left	181	0	0				
Volume Right	0	3	63				
cSH	1211	1700	697				
Volume to Capacity	0.15	0.20	0.09				
Queue Length 95th (ft)	13	0	7				
Control Delay (s)	3.6	0.0	10.7				
Lane LOS	Α		В				
Approach Delay (s)	3.6	0.0	10.7				
Approach LOS			В				
Intersection Summary							
Average Delay			3.0				
Intersection Capacity Utiliz	zation		79.7%	IC	U Level	of Service	
Analysis Period (min)			15				
, ,							

	*	<b>†</b>	7	(w	ļ	لر	<b>*</b>	×	4	4	×	t
Movement	NBL	NBT	NBR	SBL	SBT	SBR	NEL	NET	NER	SWL	SWT	SWR
Lane Configurations		4			4			4			4	
Volume (veh/h)	8	81	14	3	140	98	40	18	13	42	65	3
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.75	0.94	0.73	0.29	0.86	0.65	0.71	0.71	0.60	0.70	0.76	0.75
Hourly flow rate (vph)	11	86	19	10	163	151	56	25	22	60	86	4
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)												
pX, platoon unblocked												
vC, conflicting volume	314			105			423	386	238	410	451	96
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	314			105			423	386	238	410	451	96
tC, single (s)	4.1			4.1			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	99			99			88	95	97	88	83	100
cM capacity (veh/h)	1247			1486			462	540	801	512	496	961
Direction, Lane #	NB 1	SB 1	NE 1	SW 1								
Volume Total	116	324	103	150								
Volume Left	11	10	56	60								
Volume Right	19	151	22	4								
cSH	1247	1486	528	509								
Volume to Capacity	0.01	0.01	0.20	0.29								
Queue Length 95th (ft)	1	1	18	30								
Control Delay (s)	0.8	0.3	13.5	15.0								
Lane LOS	Α	A	В	В								
Approach Delay (s)	0.8	0.3	13.5	15.0								
Approach LOS			В	В								
Intersection Summary												
Average Delay			5.5									
Intersection Capacity Utiliz	ation		27.3%	IC	CU Level	of Service			Α			
Analysis Period (min)			15									

## APPENDIX D 2021 "Build" Traffic Conditions

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Movement	NBL	NBT	NBR	SBL	SBT	SBR	NEL	NET	NER	SWL	SWT	SWR
Lane Configurations		4			44			4			4	
Volume (veh/h)	12	130	23	3	170	98	40	18	16	54	65	3
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Hourly flow rate (vph)	13	144	26	3	189	109	44	20	18	60	72	3
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)												
pX, platoon unblocked												
vC, conflicting volume	298			170			473	447	243	462	488	157
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	298			170			473	447	243	462	488	157
tC, single (s)	4.1			4.1			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	99			100		Y	90	96	98	87	85	100
cM capacity (veh/h)	1263			1407			437	500	795	479	474	888
Direction, Lane #	NB 1	SB 1	NE 1	SW 1								
Volume Total	183	301	82	136								
Volume Left	13	3	44	60								
Volume Right	26	109	18	3								
cSH	1263	1407	501	482								
Volume to Capacity	0.01	0.00	0.16	0.28								
Queue Length 95th (ft)	1	0.00	15	29								
Control Delay (s)	0.7	0.1	13.6	15.4								
Lane LOS	Α	A	В	C								
Approach Delay (s)	0.7	0.1	13.6	15.4								
Approach LOS	0.7	0.1	В	C								
Intersection Summary												
Average Delay			4.8									
Intersection Capacity Utiliza	ation		30.2%	IC	CU Level	of Service			Α			
Analysis Period (min)			15									
			.0									

	•	•	<b>†</b>	1	<b>\</b>	<b>↓</b>			
Movement	WBL	WBR	NBT	NBR	SBL	SBT			
Lane Configurations	ሻ	7	<b>†</b>	1	*	<b>†</b>			
Volume (vph)	263	92	604	147	61	436			
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900			
Total Lost time (s)	6.0	6.0	6.0	6.0	6.0	6.0			
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00			
Frt	1.00	0.85	1.00	0.85	1.00	1.00			
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00			
Satd. Flow (prot)	1770	1583	1863	1583	1770	1863			
Flt Permitted	0.95	1.00	1.00	1.00	0.14	1.00			
Satd. Flow (perm)	1770	1583	1863	1583	269	1863			
Peak-hour factor, PHF	0.90	0.90	0.90	0.90	0.90	0.90	·		 
Adj. Flow (vph)	292	102	671	163	68	484			
RTOR Reduction (vph)	0	80	0	93	0	0			
Lane Group Flow (vph)	292	22	671	70	68	484			
Turn Type	Perm	Perm	NA	Perm	pm+pt	NA			
Protected Phases			6		5	2			
Permitted Phases	4	4		6	2				
Actuated Green, G (s)	13.9	13.9	27.3	27.3	37.7	37.7			
Effective Green, g (s)	13.9	13.9	27.3	27.3	37.7	37.7			
Actuated g/C Ratio	0.22	0.22	0.43	0.43	0.59	0.59			
Clearance Time (s)	6.0	6.0	6.0	6.0	6.0	6.0			
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0			
Lane Grp Cap (vph)	386	345	799	679	263	1104			
v/s Ratio Prot			c0.36		0.02	c0.26			
v/s Ratio Perm	c0.17	0.01		0.04	0.14				
v/c Ratio	0.76	0.06	0.84	0.10	0.26	0.44			
Uniform Delay, d1	23.3	19.7	16.2	10.8	9.5	7.1			
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00			
Incremental Delay, d2	8.2	0.1	7.8	0.1	0.5	0.3			
Delay (s)	31.5	19.8	24.0	10.9	10.0	7.4			
Level of Service	С	В	C	В	В	Α			
Approach Delay (s)	28.5		21.4			7.7			
Approach LOS	C		С			Α			
Intersection Summary									
HCM 2000 Control Delay			18.7	H	ICM 2000	Level of Ser	vice	В	
HCM 2000 Volume to Capa	acity ratio		0.81						
Actuated Cycle Length (s)			63.6		Sum of los			18.0	
Intersection Capacity Utiliza	ation		64.7%	į(	CU Level	of Service		С	
Analysis Period (min)			15						
c Critical Lane Group									

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Movement	EBL	EBT	WBT	WBR	SWL	SWR	
Lane Configurations		4	1>		¥		
Volume (veh/h)	69	482	713	3	2	166	
Sign Control		Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	
Hourly flow rate (vph)	77	536	792	3	2	184	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type		None	None				
Median storage veh)							
Upstream signal (ft)							
pX, platoon unblocked							
vC, conflicting volume	796				1483	794	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	796				1483	794	
tC, single (s)	4.1				6.4	6.2	
tC, 2 stage (s)							
tF (s)	2.2				3.5	3.3	
p0 queue free %	91				98	52	
cM capacity (veh/h)	826				125	388	
Direction, Lane #	EB 1	WB 1	SW 1				
Volume Total	612	796	187				
Volume Left	77	0	2				
Volume Right	0	3	184				
cSH	826	1700	379				
Volume to Capacity	0.09	0.47	0.49				
Queue Length 95th (ft)	8	0	66				
Control Delay (s)	2.4	0.0	23.4				
Lane LOS	Α		С				
Approach Delay (s)	2.4	0.0	23.4				
Approach LOS			С				
Intersection Summary							
Average Delay			3.7				
Intersection Capacity Utiliz	zation		87.3%	IC	U Level	of Service	)
Analysis Period (min)			15				
,							

	•	•	<b>†</b>	~	-	<b>↓</b>	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	۲	7	<b>†</b>	7	ሻ	<b>†</b>	
Volume (veh/h)	16	30	541	22	42	908	
Sign Control	Stop		Free			Free	
Grade	0%		0%			0%	
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	
Hourly flow rate (vph)	18	33	601	24	47	1009	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type			TWLTL			TWLTL	
Median storage veh)			2			2	
Upstream signal (ft)							
pX, platoon unblocked							
vC, conflicting volume	1703	601			626		
vC1, stage 1 conf vol	601						
vC2, stage 2 conf vol	1102						
vCu, unblocked vol	1703	601			626		
tC, single (s)	6.4	6.2			4.1		
tC, 2 stage (s)	5.4						
tF (s)	3.5	3.3			2.2		
p0 queue free %	93	93			95		
cM capacity (veh/h)	270	500			956		
Direction, Lane #	WB 1	WB 2	NB 1	NB 2	SB 1	SB 2	
Volume Total	18	33	601	24	47	1009	
Volume Left	18	0	0	0	47	0	
Volume Right	0	33	0	24	0	0	
cSH	270	500	1700	1700	956	1700	
Volume to Capacity	0.07	0.07	0.35	0.01	0.05	0.59	
Queue Length 95th (ft)	5	5	0	0	4	0	
Control Delay (s)	19.3	12.7	0.0	0.0	9.0	0.0	
Lane LOS	С	В			Α		
Approach Delay (s)	15.0		0.0		0.4		
Approach LOS	В						
Intersection Summary							
Average Delay			0.7				
Intersection Capacity Utiliz	ation		57.8%	IC	U Level	of Service	
Analysis Period (min)			15				
, ,							

	•	•	<b>†</b>	<b>/</b>	<b>&gt;</b>	<b>↓</b>	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	7	7	1>			4	
Volume (veh/h)	54	13	212	86	21	143	
Sign Control	Stop		Free			Free	
Grade	0%		0%			0%	
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	
Hourly flow rate (vph)	60	14	236	96	23	159	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type			None			None	
Median storage veh)							
Upstream signal (ft)							
pX, platoon unblocked							
vC, conflicting volume	489	283			331		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	489	283			331		
tC, single (s)	6.4	6.2			4.1		
tC, 2 stage (s)							
tF (s)	3.5	3.3			2.2		
p0 queue free %	89	98			98		
cM capacity (veh/h)	528	756			1228		
Direction, Lane #	WB 1	WB 2	NB 1	SB 1			
Volume Total	60	14	331	182			
Volume Left	60	0	0	23			
Volume Right	0	14	96	0			
cSH	528	756	1700	1228			
Volume to Capacity	0.11	0.02	0.19	0.02			
Queue Length 95th (ft)	10	1	0	1			
Control Delay (s)	12.7	9.9	0.0	1.2			
Lane LOS	В	A		Α			
Approach Delay (s)	12.1		0.0	1.2			
Approach LOS	В						
Intersection Summary							
Average Delay			1.9				
Intersection Capacity Utiliz	zation		35.3%	IC	U Level o	of Service	
Analysis Period (min)			15				

	•	*	<b>†</b>	<b>/</b>	<b>\</b>	<b>↓</b>	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	W		ĵ»			4	
Volume (veh/h)	13	3	210	15	4	151	
Sign Control	Stop		Free			Free	
Grade	0%		0%			0%	
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	
Hourly flow rate (vph)	14	3	233	17	4	168	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type			None			None	
Median storage veh)							
Upstream signal (ft)							
pX, platoon unblocked							
vC, conflicting volume	418	242			250		
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	418	242			250		
tC, single (s)	6.4	6.2			4.1		
tC, 2 stage (s)							
tF (s)	3.5	3.3			2.2		
p0 queue free %	98	100			100		
cM capacity (veh/h)	589	797			1316		
Direction, Lane #	WB 1	NB 1	SB 1				
Volume Total	18	250	172				
Volume Left	14	0	4				
Volume Right	3	17	0				
cSH	620	1700	1316				
Volume to Capacity	0.03	0.15	0.00				
Queue Length 95th (ft)	2	0.13	0.00				
Control Delay (s)	11.0	0.0	0.2				
Lane LOS	В	0.0	A				
Approach Delay (s)	11.0	0.0	0.2				
Approach LOS	В	0.0	J.L				
Intersection Summary							
Average Delay			0.5				
Intersection Capacity Utiliza	ation		22.0%	IC	U Level o	of Service	Α
Analysis Period (min)			15				

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Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	W		î,			4	
Volume (veh/h)	13	3	198	15	4	142	
Sign Control	Stop		Free			Free	
Grade	0%		0%			0%	
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	
Hourly flow rate (vph)	14	3	220	17	4	158	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type			None			None	
Median storage veh)							
Upstream signal (ft)							
pX, platoon unblocked							
vC, conflicting volume	395	228			237		
/C1, stage 1 conf vol							
C2, stage 2 conf vol							
Cu, unblocked vol	395	228			237		
C, single (s)	6.4	6.2			4.1		
tC, 2 stage (s)							
F (s)	3.5	3.3			2.2		
00 queue free %	98	100			100		
cM capacity (veh/h)	608	811			1330		
· · · · · · · · · · · · · · · · · · ·	WB 1	NB 1	SB 1				
Direction, Lane #		_					
/olume Total	18	237	162				
Volume Left	14	17	4				
Volume Right cSH	3 638	1700	1220				
		1700 0.14	1330				
Volume to Capacity	0.03						
Queue Length 95th (ft)	10.9	0	0.2				
Control Delay (s)	10.8	0.0					
Lane LOS	B	0.0	A				
Approach Delay (s)	10.8	0.0	0.2				
Approach LOS	В						
Intersection Summary							
Average Delay			0.6				
Intersection Capacity Utiliza	ation		21.3%	IC	U Level o	of Service	Α
Analysis Period (min)			15				

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Movement	NBL	NBT	NBR	SBL	SBT	SBR	NEL	NET	NER	SWL	SWT	SWR
Lane Configurations		4			4			4			4	
Volume (veh/h)	1	138	44	1	96	30	80	62	13	33	19	4
Sign Control		Free			Free			Stop			Stop	
Grade		0%			0%			0%			0%	
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90	0.90
Hourly flow rate (vph)	1	153	49	1	107	33	89	69	14	37	21	4
Pedestrians												
Lane Width (ft)												
Walking Speed (ft/s)												
Percent Blockage												
Right turn flare (veh)												
Median type		None			None							
Median storage veh)												
Upstream signal (ft)												
pX, platoon unblocked												
vC, conflicting volume	140			202			321	330	123	354	322	178
vC1, stage 1 conf vol												
vC2, stage 2 conf vol												
vCu, unblocked vol	140			202			321	330	123	354	322	178
tC, single (s)	4.1			4.1			7.1	6.5	6.2	7.1	6.5	6.2
tC, 2 stage (s)												
tF (s)	2.2			2.2			3.5	4.0	3.3	3.5	4.0	3.3
p0 queue free %	100			100		Y	85	88	98	93	96	99
cM capacity (veh/h)	1443			1370			611	588	928	538	594	865
Direction, Lane #	NB 1	SB 1	NE 1	SW 1								
Volume Total	203	141	172	62								
Volume Left	1	1	89	37								
Volume Right	49	33	14	4								
cSH	1443	1370	619	572								
Volume to Capacity	0.00	0.00	0.28	0.11								
Queue Length 95th (ft)	0	0	28	9								
Control Delay (s)	0.0	0.1	13.0	12.1								
Lane LOS	Α	A	В	В								
Approach Delay (s)	0.0	0.1	13.0	12.1								
Approach LOS			В	В								
Intersection Summary												
Average Delay			5.2									
Intersection Capacity Utiliza	ation		27.1%	IC	U Level o	of Service			Α			
Analysis Period (min)			15									
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	•	•	<b>†</b>	<i>&gt;</i>	<b>\</b>	Ţ		
Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	ሻ	7	<b>†</b>	7	ሻ	<b>†</b>		
Volume (vph)	152	45	337	234	64	798		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900		
Total Lost time (s)	6.0	6.0	6.0	6.0	6.0	6.0		
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00		
Frt	1.00	0.85	1.00	0.85	1.00	1.00		
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00		
Satd. Flow (prot)	1770	1583	1863	1583	1770	1863		
Flt Permitted	0.95	1.00	1.00	1.00	0.40	1.00		
Satd. Flow (perm)	1770	1583	1863	1583	750	1863		
Peak-hour factor, PHF	0.90	0.90	0.90	0.90	0.90	0.90		
Adj. Flow (vph)	169	50	374	260	71	887		
RTOR Reduction (vph)	0	42	0	141	0	0		
Lane Group Flow (vph)	169	8	374	119	71	887		
Turn Type	Perm	Perm	NA	Perm	pm+pt	NA		
Protected Phases			6		5	2		
Permitted Phases	4	4		6	2			
Actuated Green, G (s)	8.6	8.6	25.6	25.6	35.5	35.5		
Effective Green, g (s)	8.6	8.6	25.6	25.6	35.5	35.5		
Actuated g/C Ratio	0.15	0.15	0.46	0.46	0.63	0.63		
Clearance Time (s)	6.0	6.0	6.0	6.0	6.0	6.0		
Vehicle Extension (s)	3.0	3.0	3.0	3.0	3.0	3.0		
Lane Grp Cap (vph)	271	242	850	722	545	1178		
v/s Ratio Prot			0.20		0.01	c0.48		
v/s Ratio Perm	c0.10	0.00		0.07	0.07			
v/c Ratio	0.62	0.03	0.44	0.16	0.13	0.75		
Uniform Delay, d1	22.2	20.2	10.4	9.0	4.6	7.2		
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00		
Incremental Delay, d2	4.4	0.1	0.4	0.1	0.1	2.8		
Delay (s)	26.7	20.3	10.7	9.1	4.7	10.0		
Level of Service	С	С	В	Α	Α	Α		
Approach Delay (s)	25.2		10.1			9.6		
Approach LOS	С		В			Α		
Intersection Summary								
HCM 2000 Control Delay			11.6	F	ICM 2000	Level of Se	ervice B	
HCM 2000 Volume to Capa	city ratio		0.84					
Actuated Cycle Length (s)			56.1	S	um of los	t time (s)	18.0	
Intersection Capacity Utiliza	ation		60.4%			of Service	В	
Analysis Period (min)			15					
c Critical Lane Group								

	_#	<b>→</b>	+	٤	6	✓	
Movement	EBL	EBT	WBT	WBR	SWL	SWR	
Lane Configurations		ર્ન	<b>^</b>		W		
Volume (veh/h)	163	866	374	3	0	59	
Sign Control		Free	Free		Stop		
Grade		0%	0%		0%		
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	
Hourly flow rate (vph)	181	962	416	3	0	66	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type		None	None				
Median storage veh)							
Upstream signal (ft)							
pX, platoon unblocked							
vC, conflicting volume	419				1742	417	
vC1, stage 1 conf vol							
vC2, stage 2 conf vol							
vCu, unblocked vol	419				1742	417	
tC, single (s)	4.1				6.4	6.2	
tC, 2 stage (s)							
tF (s)	2.2				3.5	3.3	
p0 queue free %	84				100	90	
cM capacity (veh/h)	1140				80	636	
Direction, Lane #	EB 1	WB 1	SW 1				
Volume Total	1143	419	66				
Volume Left	181	0	0				
Volume Right	0	3	66				
cSH	1140	1700	636				
Volume to Capacity	0.16	0.25	0.10				
Queue Length 95th (ft)	14	0.20	9				
Control Delay (s)	4.1	0.0	11.3				
Lane LOS	A	0.0	В				
Approach Delay (s)	4.1	0.0	11.3				
Approach LOS	7.1	0.0	11.3 B				
• • • • • • • • • • • • • • • • • • • •							
Intersection Summary			0.0				
Average Delay	zotion		3.3	10	NII avali	of Comile-	
Intersection Capacity Utiliz	zalion		88.1%	IC	Level (	of Service	
Analysis Period (min)			15				

	•	•	<b>†</b>	<b>/</b>	<b>/</b>	<b>↓</b>	
Movement	WBL	WBR	NBT	NBR	SBL	SBT	
Lane Configurations	7	7	<b>†</b>	7	7	<b>†</b>	
Volume (veh/h)	36	30	721	22	42	657	
Sign Control	Stop		Free			Free	
Grade	0%		0%			0%	
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90	
Hourly flow rate (vph)	40	33	801	24	47	730	
Pedestrians							
Lane Width (ft)							
Walking Speed (ft/s)							
Percent Blockage							
Right turn flare (veh)							
Median type			TWLTL			TWLTL	
Median storage veh)			2			2	
Upstream signal (ft)			_				
pX, platoon unblocked							
vC, conflicting volume	1624	801			826		
vC1, stage 1 conf vol	801	001			020		
vC2, stage 2 conf vol	823						
vCu, unblocked vol	1624	801			826		
tC, single (s)	6.4	6.2			4.1		
tC, 2 stage (s)	5.4	0.2					
tF (s)	3.5	3.3			2.2		
p0 queue free %	87	91			94		
cM capacity (veh/h)	310	384			805		
· · · · · · · · · · · · · · · · · · ·			ND 4	ND 0		00.0	
Direction, Lane #	WB 1	WB 2	NB 1	NB 2	SB 1	SB 2	
Volume Total	40	33	801	24	47	730	
Volume Left	40	0	0	0	47	0	
Volume Right	0	33	0	24	0	0	
cSH	310	384	1700	1700	805	1700	
Volume to Capacity	0.13	0.09	0.47	0.01	0.06	0.43	
Queue Length 95th (ft)	11	7	0	0	5	0	
Control Delay (s)	18.3	15.3	0.0	0.0	9.7	0.0	
Lane LOS	С	С			Α		
Approach Delay (s)	16.9		0.0		0.6		
Approach LOS	С	•					
Intersection Summary							
Average Delay			1.0				
Intersection Capacity Utilizat	tion		47.9%	IC	U Level	of Service	A
mitorocoulon oupdong ounizar							

	•	•	<b>†</b>	<b>/</b>	<b>/</b>	<b>↓</b>		
Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	¥	7	ĵ.			4		
Volume (veh/h)	73	23	177	31	8	282		
Sign Control	Stop		Free			Free		
Grade	0%		0%			0%		
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90		
Hourly flow rate (vph)	81	26	197	34	9	313		
Pedestrians								
Lane Width (ft)								
Walking Speed (ft/s)								
Percent Blockage								
Right turn flare (veh)								
Median type			None			None		
Median storage veh)								
Upstream signal (ft)								
pX, platoon unblocked								
vC, conflicting volume	545	214			231			
vC1, stage 1 conf vol								
vC2, stage 2 conf vol								
vCu, unblocked vol	545	214			231			
tC, single (s)	6.4	6.2			4.1			
tC, 2 stage (s)								
tF (s)	3.5	3.3			2.2			
o0 queue free %	84	97			99			
cM capacity (veh/h)	496	826			1337			
Direction, Lane #	WB 1	WB 2	NB 1	SB 1				
Volume Total	81	26	231	322				
Volume Left	81	0	0	9				
Volume Right	0	26	34	0				
cSH	496	826	1700	1337				
Volume to Capacity	0.16	0.03	0.14	0.01				
Queue Length 95th (ft)	14	2	0.14	1				
Control Delay (s)	13.7	9.5	0.0	0.3				
Lane LOS	13.7 B	3.5 A	0.0	Α				
Approach Delay (s)	12.7	7	0.0	0.3				
Approach LOS	12.7 B		0.0	0.0				
Intersection Summary								
Average Delay			2.2					
Intersection Capacity Utiliza	ation		32.0%	IC	U Level	of Service	Α	
Analysis Period (min)			15					

	•	•	<b>†</b>	<b>/</b>	<b>/</b>	<b>↓</b>		
Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	¥		ĵ»			ર્ન		
Volume (veh/h)	35	9	163	37	10	255		
Sign Control	Stop		Free			Free		
Grade	0%		0%			0%		
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90		
Hourly flow rate (vph)	39	10	181	41	11	283		
Pedestrians								
Lane Width (ft)								
Walking Speed (ft/s)								
Percent Blockage								
Right turn flare (veh)								
Median type			None			None		
Median storage veh)								
Upstream signal (ft)								
pX, platoon unblocked								
vC, conflicting volume	507	202			222			
vC1, stage 1 conf vol								
vC2, stage 2 conf vol								
vCu, unblocked vol	507	202			222			
tC, single (s)	6.4	6.2			4.1			
tC, 2 stage (s)								
tF (s)	3.5	3.3			2.2			
p0 queue free %	93	99			99			
cM capacity (veh/h)	521	839			1347			
			CD 4					
Direction, Lane #	WB 1	NB 1	SB 1					
Volume Total	49	222	294					
Volume Left	39	0	11					
Volume Right	10	41	0					
cSH	565	1700	1347					
Volume to Capacity	0.09	0.13	0.01					
Queue Length 95th (ft)	7	0	1					
Control Delay (s)	12.0	0.0	0.4					
Lane LOS	В		A					
Approach Delay (s)	12.0	0.0	0.4					
Approach LOS	В							
Intersection Summary								
Average Delay			1.2					
Intersection Capacity Utiliz	ation		31.5%	IC	U Level of	of Service	Α	
Analysis Period (min)			15					

	•	•	<b>†</b>	<b>/</b>	<b>\</b>	ţ		
Movement	WBL	WBR	NBT	NBR	SBL	SBT		
Lane Configurations	¥		ĵ»			ર્ન		
Volume (veh/h)	35	9	135	37	10	230		
Sign Control	Stop		Free			Free		
Grade	0%		0%			0%		
Peak Hour Factor	0.90	0.90	0.90	0.90	0.90	0.90		
Hourly flow rate (vph)	39	10	150	41	11	256		
Pedestrians								
Lane Width (ft)								
Walking Speed (ft/s)								
Percent Blockage								
Right turn flare (veh)								
Median type			None			None		
Median storage veh)								
Upstream signal (ft)								
pX, platoon unblocked								
vC, conflicting volume	448	171			191			
vC1, stage 1 conf vol								
vC2, stage 2 conf vol								
vCu, unblocked vol	448	171			191			
tC, single (s)	6.4	6.2			4.1			
tC, 2 stage (s)								
tF (s)	3.5	3.3			2.2			
p0 queue free %	93	99			99			
cM capacity (veh/h)	564	873			1383			
Direction, Lane #	WB 1	NB 1	SB 1					
Volume Total	49	191	267					
Volume Left	39	0	11					
Volume Right	10	41	0					
cSH	608	1700	1383					
Volume to Capacity	0.08	0.11	0.01					
Queue Length 95th (ft)	7	0	1					
Control Delay (s)	11.4	0.0	0.4					
Lane LOS	В	0.0	A					
Approach Delay (s)	11.4	0.0	0.4					
Approach LOS	В							
Intersection Summary								
Average Delay			1.3					
Intersection Capacity Utiliz	zation		30.2%	IC	U Level o	of Service	Α	
Analysis Period (min)			15					

## APPENDIX 2



July 31, 2014

Pastime Amusement Company 211 King Street, Suite 300 Charleston, South Carolina 29401

C/o: Mr. Steve Dudash

Via email: <a href="mailto:sdudash@davisfloyd.com">sdudash@davisfloyd.com</a>

RE: Jurisdictional Wetland/Waters of the United States Delineation 70.37 Acre Tuxbury Tract TMS #263-00-04-001
Cainhoy, Berkeley County, South Carolina

Dear Mr. Dudash:

The field delineation of jurisdictional wetlands/waters of the United States located within the above referenced tract has been completed and subsequently surveyed by Thomas & Hutton, Inc. The delineated jurisdictional wetlands/waters of the United States identified include both freshwater wetlands and critical area which are of common distribution throughout the lower coastal plain of South Carolina. These areas were identified and delineated in the field in accordance with the directives of the U.S. Army Corps of Engineers 1987 Wetlands Delineation Manual and the October 2008 Regional Supplement to the Corps of Engineers Wetland Delineation Manual: Atlantic and Gulf Coastal Plain Region.

The delineation of on-site critical areas was largely based on the presence of saltwater tolerant vegetation and exposure to the normal daily tidal cycle. Freshwater wetland areas were delineated based upon the presence of hydric soils, hydrophitic vegetation and near surface wetland hydrology. All three of these parameters are required to be present for wetland boundary determination.

The attached review exhibit prepared by Thomas & Hutton Engineering Company depicting the surveyed jurisdictional wetland/waters of the United States boundaries is an accurate representation of the field delineation that was performed by Red Bay Environmental and represents the extent of wetlands within the tract boundaries. The delineation of the tract resulted in 2.62 acres of on-site freshwater wetlands and 6.83 acres of critical area. We are currently in progress on seeking verification of the on-site wetlands/waters of the United States delineation from the US Army Corps of Engineers and certification of the delineated on-site critical area boundaries from the SCDHEC Office of Ocean and Coastal Resource Management.

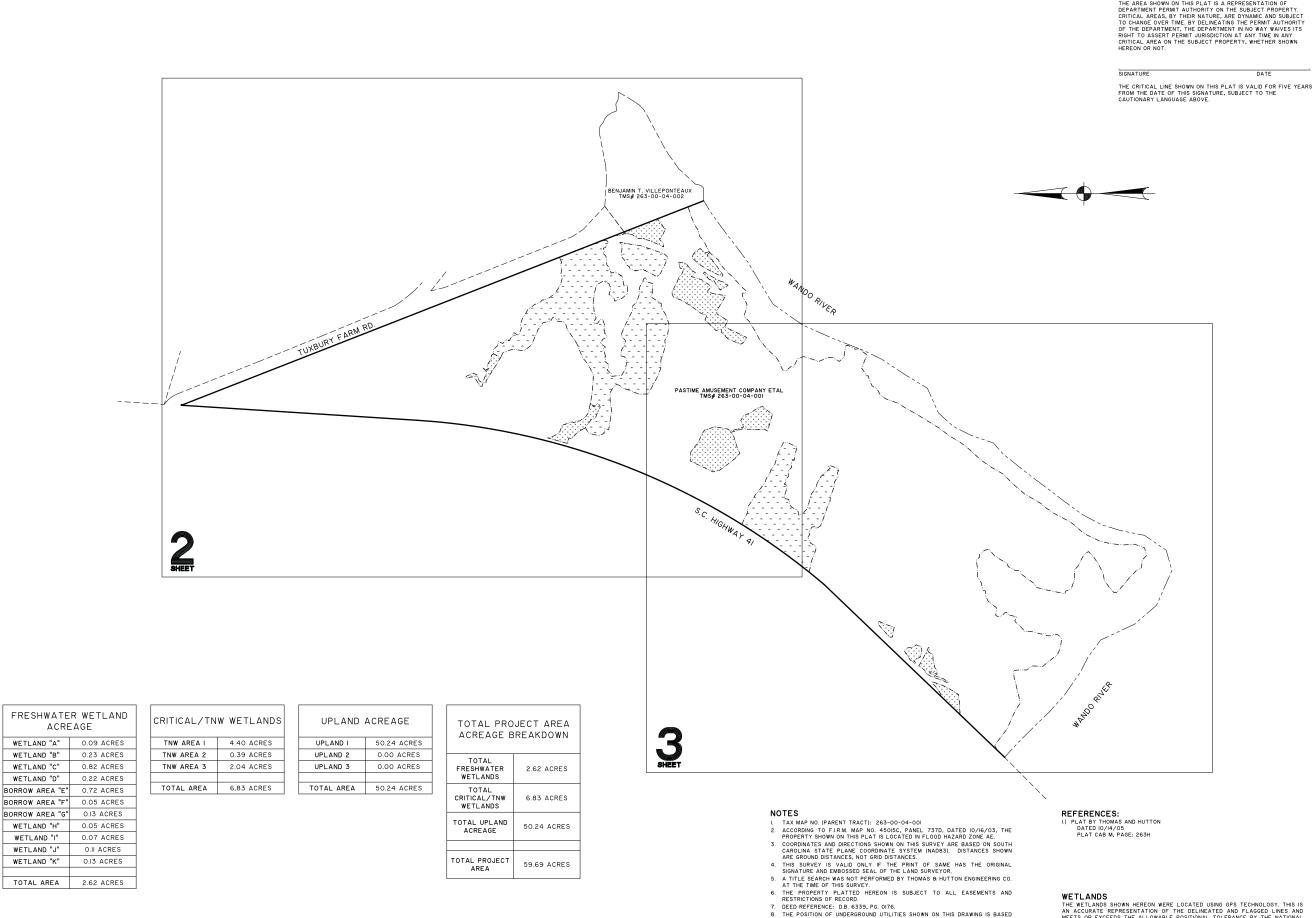
Please contact me at (843) 810-3311 with any questions regarding this material. We will keep you posted on the continued regulatory coordination on this project with regards to the US Army Corps

of Engineers and the SCDHEC Office of Ocean and Coastal Resource Management. Thank you for the opportunity of continuing to assist you with the Natural Resources services associated with the project.

Sincerely,

Judson A. Goff

Attachments: Wetland Survey (Review) Exhibit prepared by Thomas & Hutton Engineering Co.



AREA

ACREAGE

TOTAL AREA 2.62 ACRES

WETLAND "A"

WETLAND "B"

WETLAND "C"

WETLAND "D"

BORROW AREA "E"

WETLAND "H"

WETLAND "I"

WETLAND "K"

WETLAND "J"

VICINITY MAP This document and all reproducible copies of this document are the property of Thomas & Hutton. Reproduction of this document in ot permitted without written consent of Thomas & Hutton unles this document becomes a matter of public record. ALTERATION: TO THIS DOCUMENT ARE NOT PERMITTED.

#### LEGEND

BENCHMARK

MEANDER POINT (NO MONUMENT)

CONCRETE MONUMENT (FOUND)
CONCRETE MONUMENT (SET)
IRON PIPE (FOUND)
IRON PIPE (FOUND)
IRON PIPE (SET)
IRON REBAR (FOUND)
IRON REBAR (SET)
CITICAL/TINW WETLANDS AREA
WETLANDS AREA

THOMAS 8 HUTTON ENGINEERING CO. No. COO285



I HEREBY STATE THAT TO THE BEST OF MY PROFESSIONAL KNOWLEDGE, INFORMATION, AND BELIEF, THE SURVEY SHOWN HEREON WAS MADE IN ACCORDANCE WITH REQUIREMENTS OF THE STANDARDS OF PRACTICE MANUAL FOR SURVEYING IN SOUTH CAROLINA, AND MEETS OR EXCEEDS THE REQUIREMENTS FOR A CLASS "A" SURVEY AS SPECIFIED THEREIN.

F. ELLIOTTE QUINN III SOUTH CAROLINA PROFESSIONAL LAND SURVEYOR LICENSE NO. 10292

WETLAND SURVEY

### OF TRACT A CONTAINING 70.37 AC.

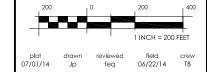
NEAR CAINHOY BERKELEY COUNTY. S.C.

PASTIME AMUSEMENT COMPANY

No.	Revision	Ву	Date

# THOMAS & HUTTON Engineering | Surveying | Planning | GIS | Consulting

682 Johnnie Dodds Blvd., Suite 100 PO Box 1522 Mt. Pleasant, SC 29465-1522 p 843.849.0200 f 843.849.0203



SHEET 1 OF 4

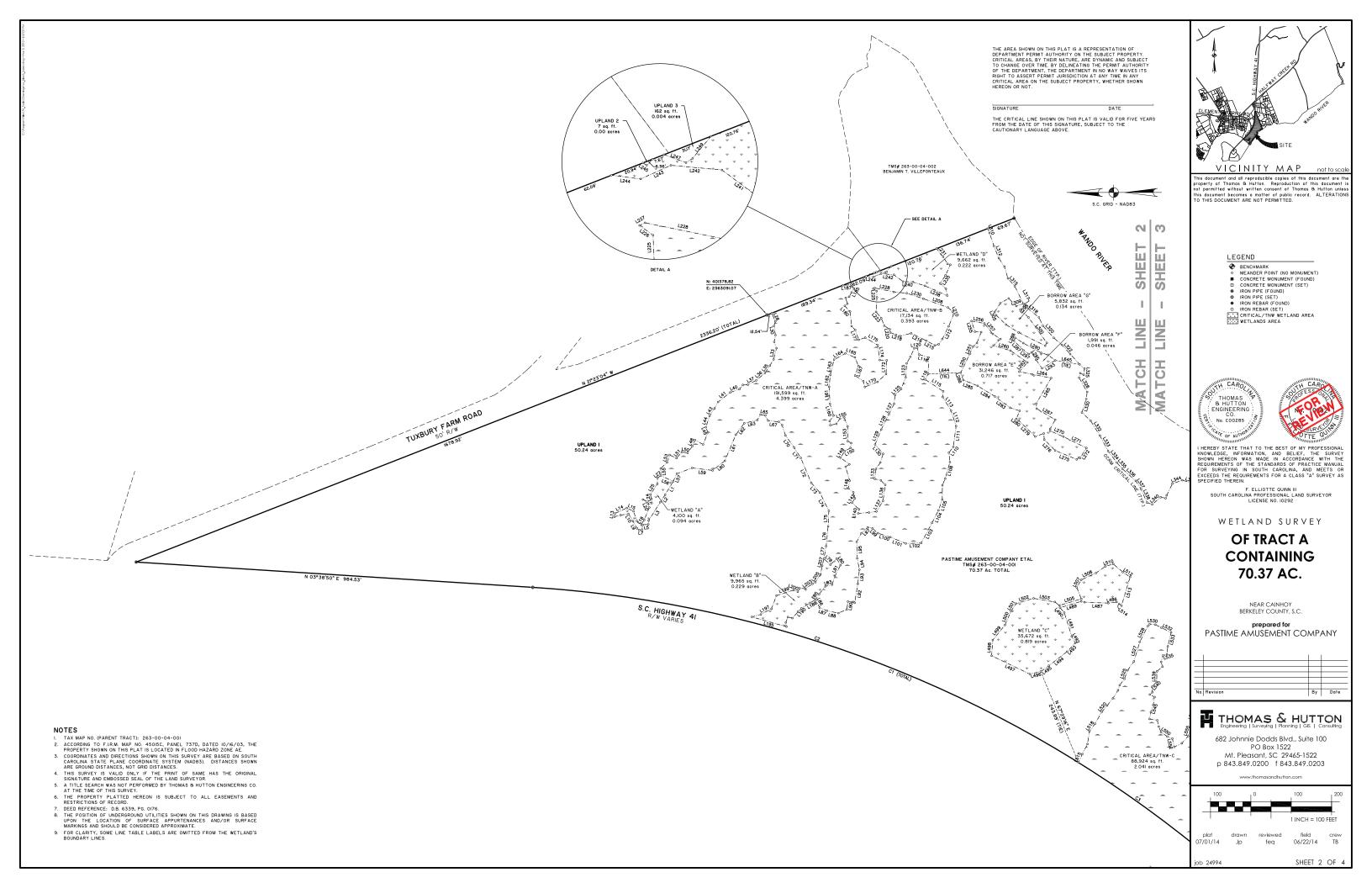
WETLANDS

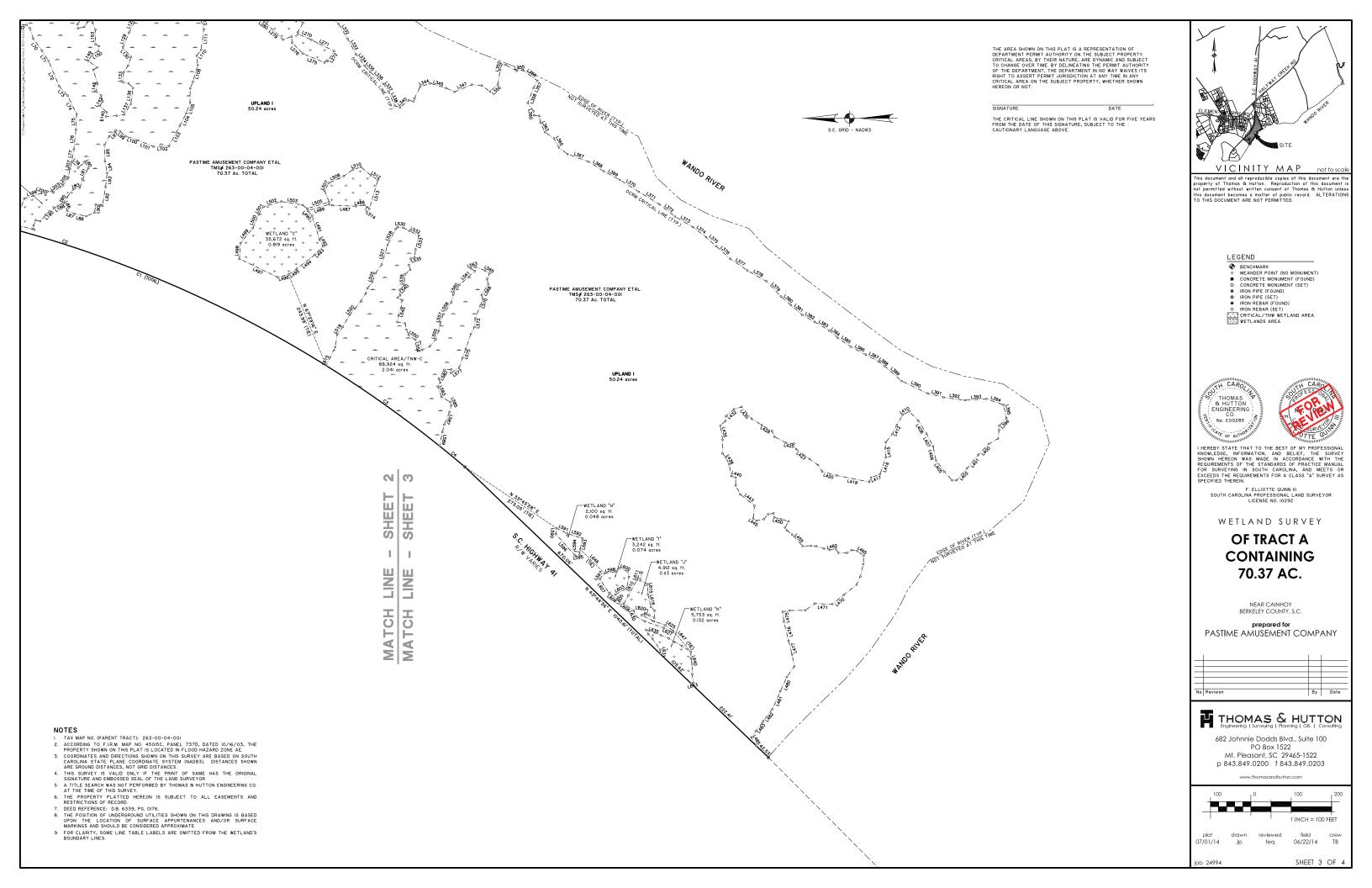
B. THE POSITION OF UNDERGROUND UTILITIES SHOWN ON THIS DRAWING IS BASED UPON THE LOCATION OF SURFACE APPURTENANCES AND/OR SURFACE MARKINGS AND SHOULD BE CONSIDERED APPROXIMATE.

9. FOR CLARITY, SOME LINE TABLE LABELS ARE OMITTED FROM THE WETLAND'S BOUNDARY LINES.

WE ILANDS
THE WETLANDS SHOWN HEREON WERE LOCATED USING GPS TECHNOLOGY. THIS IS
AN ACCURATE REPRESENTATION OF THE DELINEATED AND FLAGGED LINES AND
MEETS OR EXCEEDS THE ALLOWABLE POSITIONAL TOLERANCE BY THE NATIONAL
MAP ACCURACY STANDARDS. THESE WETLANDS ARE UNDER THE JURISDICTION AND
PERMITTING AUTHORITY OF THE U.S. ARMY CORPS OF ENGINEERS AND/OR S.C.
OFFICE OF OCEAN AND COASTAL RESOURCE MANAGEMENT.

THE AREA SHOWN ON THIS PLAT IS A REPRESENTATION OF





INE	LINE TABLE BEARING	LENGTH
J	N 58°52'43" W	38.64
.2	N 56°44'54" W N 57°41'17" W	2I.73' 54.I4'
_4	N 85°10'08" W	9.38
_5 _6	N 04°57'38" W N 82°58'34" W	14.16 <sup>1</sup>
_6 _7	N 03°49'37" E	6.81
_8	N 34°48'41" F	6.63'
.9 .10	N 60°55'15" E N 57°58'51" E	20.40'
.11	N 07°51'45" W	19.78
.12	N 15°22'20" W	15.83
.13	S 80°02'45" E S 24°51'44" E	8.36' 32.09'
.15	S 25°30'36" W	18.48
_16 _17	S 70°48'42" W S 32°47'35" W	25.64 <sup>1</sup>
.18	S 54°53'07" E	12.13
.19	S 67°51'38" E	33.45
.20 .21	N 67°09'24" E N 39°25'50" E	10.82
.22	S 22°18'26" W	23.30
.23	N 88°06'08" E	10.51
.24	N 75°07'I0" E S 56°39'I6" E	11.19 <sup>1</sup> 31.59 <sup>1</sup>
.26	S 88°52'43" E	14.39
.27	S 37°05'06" E	10,27
.28 .29	S 66°57'16" W N 73°46'00" W	22.27' II.59'
.30	S 81°04'19" W	23.30
.3I	N 79°17'16" W	16.82
.32	N 75°19'55" W	16.76' 28.63'
.34	N 59°00'15" W	18.24
.35 .36	N 56°32'35" W N 39°53'50" W	21.70° 28.49°
.37	N 27°38'50" W	23.17'
.38	N 02°07'24" W	12.33
.39	N 50°47'27" W N 19°56'57" W	13.46' 24.39'
41	N 38°13'02" W	38.33'
42	N 61°21'05" W	18.20'
.43	N 71°39'08" W	22.38' 29.42'
.45	S 67°45'30" W	13.62
.46 47	N 68°29'29" W N 28°31'31" E	32.17' 23.13'
.47 .48	N 67°29'25" W	16.15
49	N 55°06'II" W	20.92
.50 .5I	N 08°48'51" E N 48°35'12" W	14.30° 20.17°
52	N 24°40'17" E	18.86
.53	N 71°14'41" W	19.42
.54 .55	N 43°52'59" W S 89°28'19" W	21.87' 17.38'
.56	S 25°29'09" W	33.99'
.57 .58	S 64°39'26" E S 20°42'II" E	21.04 <sup>1</sup> 40.68 <sup>1</sup>
.58	S 06°45'42" W	40.68° 51.15°
.60	S 38°I6'48" E	38.31
.6I .62	S 67°04'48" E S 53°41'23" E	70.33 <sup>1</sup> 35.00 <sup>1</sup>
.63	S 13°52'12" E	33.49
.64	S 59°51'41" E	15.57
.65 .66	S 10°26'25" W S 61°38'43" W	12.24 <sup>1</sup> 14.47 <sup>1</sup>
67	S 06°24'43" W	26.84
.68 .69	S 45°00'12" W S 71°59'02" W	II.14' 27.06'
70	S 54°24'48" W	37.21
.71	S 57°19'37" W	30.41
.72 .73	S 67°15'32" W S 48°27'05" W	67.00' 32.04'
74	S 63°48'58" W	50.52
75 76	N 87°24'40" W	38.44
.76 .77	N 84°10'59" W N 80°09'44" W	49.54' 31.39'
.78	S 42°44'50" W	21.69
.79 80	S 43°49'46" E S 60°45'53" W	21.95 <sup>1</sup> 18.74 <sup>1</sup>
.80 .8I	N 63°02'25" W	30.54
.82	N 72°03'07" W	00.07
.83 .84	N 14°15'28" W N 51°22'26" W	17.19 <sup>1</sup> 25.02 <sup>1</sup>
85	N 57°39'04" W	15.93
.86	S 63°16'23" W	22.11
87 88	S 23°24'59" W S II°19'19" W	19.70' 29.03'
89	S 23°26'00" E S 81°43'35" E	22.49
.90 .9I		19.79 <sup>1</sup>
.91 .92	S 80°35'54" E	16.94° 47.62'
93	S 83°32'42" F	34.99
.94 .95	N 79°08'43" E N 88°15'16" E	28.71 <sup>1</sup> 40.99 <sup>1</sup>
.95 .96	S 61°25'42" E	24.40
.97	S 42°19'57" E	21.55
98	S II°55'29" W S 4I°32'I5" W	II.59'
.100	S 17°42'06" W	18.20' 32.66'
.101	S 22°19'06" W	41.04
102	S 01°47'00" E S 61°48'39" E	38.22' 56.93'
.104	S 62°39'IO" E	34.73
.105	S 70°41'37" E	28.16
.106 .107	S 89°24'56" E S 67°08'52" E	35.54 <sup>1</sup>
.108	S 73°54'10" E	42.69'
109		23.42
.IIO .III	N 83°37'43" E S 52°56'19" E S 82°23'35" E N 71°52'40" F	18.II' 51.91'
.III .II2		40.36
.113	N 58°26'41" E	39.45
.114	S 84°56'01" E	14.34
.II5 .II6	S 62°43'44" F	53.31 <sup>1</sup>
.117	S 87°58'37" E	40.53
	N 17°38'45" E	24.81
118 119	N 73°34'06" E	16.91

LINE	LINE TABLE BEARING	LENGTH
LI2I	N 65°21'49" W	23.48
LI22 LI23	N 60°39'34" W N 85°52'24" W	18.49 34.60
LI24	N 69°00'24" W	30.99
LI25	N 44°32'35" W	21.18
LI26 LI27	N 83°27'05" W N 63°18'03" W	22.I5 28.73
LI28	N 63°22'II" W	42.55
LI29 LI30	N 67°44'14" W S 49°06'07" W	39.88
LI30 LI3I	N 71°40'43" W	30.64 22.82
LI32	N 56°04'53" W	19.02
LI33 LI34	N 83°01'31" W S 13°30'41" W	24.88 I5.56
LI35	S 46°02'29" W	15.54
LI36 LI37	N 82°07'03" W N 58°28'08" W	39.94
LI37 LI38	N 07°57'12" W	30.96 I8.9I
LI39	N 04°20'22" W	26.70
LI40 LI4I	S 78°46'50" E N 43°20'25" E	10.39 23.60
LI42	S 56°53'24" E	12,83
LI43 LI44	N 75°39'26" E N 38°10'11" E	15.57 15.75
LI45	S 80°15'33" E	19.25
LI46	N 73°50'44" E	36.07
LI47 LI48	S 33°05'46" E N 37°06'10" E	10.9 27.34
LI49	S 56°50'39" E	19.24
LI50 LI5I	S 28°49'10" E S 82°25'16" E	16.34 12.21
LI52	N 30°25'04" E	10.01
LI53	N 89°39'09" E	36.06
LI54 LI55	N 15°35'20" W	23.97 II.27
LI56	N 55°59'40" W	15.60
LI57 LI58	N 12°20'30" W N 81°32'36" E	I5.3€ I0.I7
LI59	S 55°15'39" E	16.85
LI60	N 73°03'07" E N 87°03'05" E	30.29
LI61 LI62	S 84°25'33" E	42.50 29.55
LI63	S 76°04'21" E	38.73
LI64 LI65	\$ 29°03'17" E \$ 22°51'09" W	32.26 25.54
LI66	S 68°01'56" W	23.27
LI67 LI68	N 70°31'13" W S 34°15'41" W	24.90 24.49
L169	S 74°42'27" W	15.13
LI70	S 21°57'02" E	33.94
LI7I LI72	S 42°44'I0" E S 87°I5'02" E	28.69 33.89
LI73	N 02°46'29" E	17.4
L174 L175	N 82°20'29" E N 31°17'28" E	37.0 36.I8
LI76	N 18°49'42" W	16,95
LI77 LI78	N 70°02'39" E N 46°19'28" E	26.04
L178 L179	N 46°19'28" E N 84°05'59" E	12.77 36.50
LIBO	N 46°49'48" E	19.30
LI8I LI82	S 39°57'21" E N 74°42'46" E	8.3 I5.22
LI83	S 17°25'26" E	8.82
LI84 LI85	S 60°12'17" E S 58°55'05" E	12.20 11.52
LI86	N 53°08'49" E	11.40
LI87 LI88	N 03°04'15" W N 29°52'15" W	20.54 16.08
LI89	N 32°29'04" W	24.98
LI90 LI9I	N 45°38'I2" W N 48°I2'00" W	12.84 20.36
L191	N 13°23'01" E	11.62
L193	N 69°12'47" W	14.25
LI94 LI95	S 81° 02'42" W N 15° 44'22" E	10.63 89.03
LI96	S 15°26'05" E	22.88
LI97 LI98	S 28°18'25" E S 69°11'12" E	30.19 34.86
LI99	S 17°32'44" F	43.96
L200	S 20°08'34" W S 62°21'47" E	II.48 9.68
L202	S 03°02'06" W	14.10
L203	S 33°33'21" E S 30°46'22" E	21.74 7.78
L204	S 56°24'02" E	23,3€
L206	S 78°55'38" E	21.7
L207	S 75°53'48" E S 19°31'45" W	17.77 64.60
L209	S 41°26'52" W	15.86
L2I0 L2II	S 67°35'54" W N 67°30'33" W	6,62 32.53
L2I2	N 63°23'31" W	35.4
L213	N 55°27'47" W N 16°40'30" W	15.6
L2I4 L2I5	N 28°46'49" E	10.03 24.48
L216	N 26°05'59" E	41.53
L217 L218	N 14°38'15" W N 17°23'01" E	28.04 10.90
L219	N 22°21'02" E	15.22
L220	N 80°II'49" E	7.9
L221	N 33°09'I6" E N 68°25'31" E	16.25 20.29
L223	N 50°03'49" E	20.10
L224 L225	S 86°31'10" E N 87°32'40" E	36.2 15.38
L225	N 36°03'41" E	10.35
L227	S 25°40'55" E	3.78
L228 L229	S II°34'54" W S 05°43'40" W	48.47 32.08
L230	S 18°18'04" W	43.3€
L231	N 50°53'22" E S 58°08'14" W	25.97 20.78
L232 L233	S 17°32'55" W	7.2
L234	N 65°34'45" W	29.25
L235 L236	N 56°42'44" W S 42°13'39" W	23.87 19.16
	S 79°00'33" W	17.27
L237		
L238 L239	N 23°36'19" E N 17°43'52" E	60.29 31,39

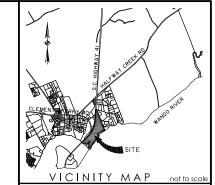
LINE	LINE TABLE BEARING	LENGTH
L241 L242	N 36°49'08" E N 05°13'45" E	28.08 <sup>1</sup> 31.78 <sup>1</sup>
L243	N 24°18'35" W	20.57
L244 L245	N 07°19'25" E S 32°25'44" W	18.22' 2.67'
L246	S 45°41'35" E	5.24'
L247 L248	S 20°06'30" W N 32°52'54" W	14.46' 4.90'
L249 L250	S 50°22'41" E S 64°31'32" E	17.75' 51.29'
L25I	S 65° 47'10" E	19.74
L252 L253	S 42°38'24" E S 68°30'54" E	13.52' 29.05'
L254	N 03°47'23" E	15.68
L255 L256	N 72°28'49" E S I0°25'48" W	27.73' 32.44'
L257 L258	S 51°08'53" W S 33°50'02" W	33.45' 22.73'
L259	N 42°48'16" W	23.72
L260 L261	S 16°32'34" W S 34°50'03" W	43.76' 5l.46'
L262 L263	N 48°24'10" W S II°50'08" W	30.37' 32.44'
L264	S 10°59'11" W	48.10'
L265 L266	N 59°47'53" W S 84°10'08" W	73.62' I2.54'
L267 L268	S 30°47'14" W N 61°11'00" W	53.24
L269	N 88°35'16" W	26.03' 4.82'
L270 L271	S 23°25'58" W S 26°17'07" W	36.2I' 63.24'
L272	N 57°55'06" W	29.42'
L273 L274	N 26°14'II" E N 39°32'03" W	3.0l <sup>1</sup> 7.34 <sup>1</sup>
L275	N 22°25'40" E N 45°11'05" E	57.77' 38.20'
L277	N 85°07'49" E	15.12
L278 L279	N 20°00'25" W N 43°58'48" E	22.35 <sup>'</sup> 56.93 <sup>'</sup>
L280 L28I	N 36°39'46" E S 67°34'02" E	7.41' 21.46'
L282	N 17°51'35" E	24.70
L283 L284	N 36°33'05" E N 31°25'01" E	47.47' 49.78'
L285	N 22°06'44" E	38.34
L286 L287	N 45°13'19" E	19.27' 33.73'
L288 L289	S 66°08'42" E S 32°57'27" W	7.88 <sup>1</sup> 23.69 <sup>1</sup>
L290	S 28°42'27" W	50.88
L291 L292	S 15°53'51" W S 37°28'47" W	17.II' 22.74'
L293 L294	N 30°57'28" W N 54°II'I8" E	37.86
L295	N 58°44'23" E	25.95' 2l.27'
L296 L297	N 29°54'17" W N 34°19'02" E	7,81 <sup>1</sup>  5.69
L298	N 49°00'16" W	14.50'
L299 L300	S 43°18'24" W S 54°19'16" W	27.88' 77.73'
L301 L302	N 59°28'53" W N 26°22'26" E	8.IO' 73.80'
L303	N 32°16'30" E	36.20
L304 L305	N 43°22'00" E N 65°29'45" E	33.65 <sup>'</sup> 9.53 <sup>'</sup>
L306 L307	S 56°40'19" E S 29°37'56" E	25.58' 23.86'
L308	S 44°59'27" W	26.69
L309 L3I0	S 18°25'05" E S 70°10'55" W	18.51' 11.97'
L3II	S 71°19'50" W	33.94'
L3I2 L3I3	S 68°04'37" W S 56°21'12" W	32.47' 25.40'
L3I4 L3I5	S 73°33'03" W S 48°52'33" W	30.20' 25.65'
L316	S 63°41'II" W	48.43'
L317 L318	S 63°41'II" W S 39°40'I7" W	4.30' 47.50'
L319	S 64°14'46" W	23.03
L320 L321	S 40°43'57" W	40.05' 26.40'
L322 L323	S 47°54'37" W S 47°31'26" W	30.80' 34.82'
L324	S 40°42'37" W	15.62
L325 L326	N 83°39'52" W N 24°46'12" E	15,72' 9.71'
L327 L328	N 76°42'43" W S 60°27'21" W	II.55'
L329	N 82°48'24" W	40.36' 17.66'
L330 L331	N 72°14'24" W S 43°24'06" W	35.20' 29.48'
L332	S 58°01'14" W	43.53
L333 L334	S 61°59'52" W S 52°52'05" W	43.28' 35.94'
L335	S 48°27'II" W	20.46
L336 L337	S 42°01'34" W S 56°51'07" W	44.67' 24.38'
L338 L339	S 66°20'48" W S 19°52'01" W	36.35'  3.79
L340	S 39°59'05" E	27.62'
L34I L342	S II°33'28" W S 69°31'39" E	12.29' 7.62'
L343 L344	S 64°01'25" E S 19°32'27" E	3I.96' 26.14'
L345	S 16°26'02" W	41.33'
L346 L347	S 24°06'55" W S 22°45'49" E	23.19' 46.22'
L348	S 05°06'09" W	24.54
L349	S 42°56'31" E	25.7I' 26.08'
L350	S 80°23'46" E	36.25'  4.19
L351	S 75°23'21" E 1	14.13
L351 L352 L353	S 75°23'21" E S 06°58'25" W	9.58'
L351 L352 L353 L354	S 06°58'25" W S 28°04'19" W	31.73
L351 L352 L353 L354 L355 L356	S 06°58'25" W S 28°04'19" W S 08°11'12" E S 35°51'54" W	31.73' 14.53' 45.09'
L351 L352 L353 L354 L355	S 06°58'25" W S 28°04'19" W S 08°11'12" E	31.73' 14.53'

LINE	LINE TABLE BEARING	LENGTH
L361	S 06°21'57" W	12.74
L363	S 78°38'42" W S 65°01'48" W	16.94' 26.34'
L364	S 34°09'39" W	26.93
L365 L366	S 61°31'43" W S 37°41'58" W	25.8l <sup>1</sup> 26.44 <sup>1</sup>
L367	S 20°04'24" W S 32°04'18" W	56.22'
L368 L369	S 28°17'27" W	44.18' 44.48'
L370	S 31°57'58" W	55.98'
L371 L372	S 31º16'30" W S 38º27'56" W	60.59' 48.44'
L373	S 30°13'28" W	51.30
L374 L375	S 37°28'36" W S 42°02'04" W	41.32' 33.80'
L376	S 41°49'29" W	45.81
L377	S 34°13'46" W S 29°34'57" W	51.97' 54.52'
L379	S 46°25'34" W	51.99
L380	S 40°50'32" W S 40°37'00" W	32.55' 37.16'
L382	S 29°29'49" W	35.40
L383 L384	S 30°40'33" W S 40°40'01" W	4I.98' 28.01
L385	S 34°06'27" W	39.57
L386 L387	S 27°45'56" W S 28°26'27" W	41.51 <sup>1</sup> 36.82 <sup>1</sup>
L388	S 37°15'23" W	17.84
L389 L390	S 41°15'29" W S 25°26'09" W	56.04
L390	S 13°53'39" W	7l.80 <sup>1</sup> 39.96 <sup>1</sup>
L392	S 07°41'47" W	53.66
L393 L394	S 19°20'12" W	53.29' 44.91'
L395	S 77°32'07" W	33.54
L396 L397	N 87°06'26" W	26.01 <sup>1</sup>
L398	N 83°03'08" W	21.20'
L399 L400	N 30°10'27" W N 45°59'59" W	26.43' 37.52'
L40I	N 50°13'19" W	43.73'
L402 L403	N 48°38'01" W N 00°18'54" W	39.19' II.16'
L404	N 48°23'58" E	28.26'
L405	N 53°12'26" E N 78°26'20" E	35.20' 35.20'
L407	N 62°20'08" E	35.77'
L408 L409	N 57°36'58" E N 46°21'27" E	37.98' 32.12'
L410	N 27940'51" W	18,57
L4II L4I2	N 60°12'11" W N 63°43'10" W	28.57' 26.01'
L413	N 51°00'16" W	25.71
L414 L415	N 85°42'48" W S 86°04'47" W	15.20' 22.12'
L416	N 70°34'22" W	44,33'
L417 L418	N 20°52'21" W N 68°05'17" W	23.58' II.64'
L419	N IIº16'48" E	82.87'
L420 L421	N 15°21'04" E N 57°45'19" E	37.03 <sup>1</sup> 18.76 <sup>1</sup>
L422	IN 35°08'08" E	26.01
L423 L424	N 36°47'49" E N 66°46'28" E	41.25' 14.43'
L424	N 06°05'20" E	19.45
L426	N 27°54'50" E	32.32'
L427 L428	N 65°58'16" E N 30°00'08" E	15.89' 29.10'
L429	N 31°27'05" E N 49°42'34" E	29.00'
L430 L431	N 49°42'34" E N 17°03'19" W	39.00' 19.52'
L432	N 40°38'36" W	26.50'
L433 L434	N 85°13'54" W N 43°06'29" W	II.93' I7.22'
L435	S 81°06'13" W	35.18'
L436 L437	N 89°04'26" W S 49°58'22" W	33.70 <sup>1</sup>
L438	C 63037'00" W	19.93'
L439 L440	S 79°33'20" W S 18°56'52" W	29.46' II.66'
L44I	N 89°06'20" W	19.24
L442 L443	S 62°44'25" W S 38°49'54" W	25.12'
L444	N 84°43'49" W	44.86 <sup>1</sup> 3l.80 <sup>1</sup>
L445	S 33°04'14" W S II°13'32" E	9.81
L446		
L447	S 50°03'04" E	18.68 <sup>1</sup>
L448	S 50°03'04" E S 09°17'34" E	15.98 <sup>1</sup> 13.81 <sup>1</sup>
	\$ 50°03'04" E \$ 09°17'34" E \$ 79°21'04" W	15.98 <sup>1</sup> 13.81 <sup>1</sup> 10.24 <sup>1</sup>
L448 L449 L450 L451	S 50°03'04" E S 09°17'34" E S 79°21'04" W S 14°24'15" W S 16°37'26" W	15.98' 13.81' 10.24' 17.34' 19.24'
L448 L449 L450 L451 L452	S 50°03'04" E S 09°17'34" E S 79°21'04" W S 14°24'15" W S 16°37'26" W N 60°52'28" W	15.98'   13.81'   10.24'   17.34'   19.24'   17.57'
L448 L449 L450 L451 L452 L453 L454	\$ 50°03'04" E \$ 09°17'34" E \$ 79°21'04" W \$ 14°24'15" W \$ 16°37'26" W N 60°52'28" W \$ 57°14'43" W \$ 37°34'49" W	15.98'   13.81'   10.24'   17.34'   19.24'   17.57'   8.83'   16.00'
L448 L449 L450 L451 L452 L453 L454 L455	S 50°03'04" E S 09°17'34" E S 79°21'04" W S 14°24'15" W S 16°37'26" W N 60°52'28" W S 57°14'43" W S 37°34'49" W S 47°48'59" W	15.98' 13.81' 10.24' 17.34' 19.24' 17.57' 8.83' 16.00' 38.75'
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457	\$ 50°03'04" E \$ 09°17'34" E \$ 79°21'04" W \$ 14°24'15" W \$ 16°37'26" W N 60°52'28" W \$ 57°14'43" W \$ 37°34'49" W \$ 47°48'59" W \$ 0°51'32" E \$ 03°59'44" W	15.98' 13.81' 10.24' 17.34' 19.24' 17.57' 8.83' 16.00' 38.75' 20.70'
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457 L458	\$ 50°03'04" E \$ 09°17'34" E \$ 79°21'04" W \$ 14°24'15" W \$ 16°37'26" W \$ 57°14'43" W \$ 37°34'49" W \$ 74°45'59" W \$ 00°51'32" E \$ 03°59'44" W	15.98' 13.81' 10.24' 17.34' 19.24' 17.57' 8.83' 16.00' 38.75' 20.70' 12.96'
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457	\$ 50°03'04" E \$ 09°17'34" E \$ 09°17'34" E \$ 79°2!'04" W \$ 14°24'15" W \$ 16°37'26" W \$ 57°14'43" W \$ 47°48'59" W \$ 90°51'32" E \$ 03°59'44" W \$ 17°34'09" W \$ 13°30'30" W \$ 10°58'40" E	15.98'   13.81'   10.24'   17.34'   19.24'   17.57'   8.83'   16.00'   38.75'   20.70'   12.96'   19.79'   14.86'   15.67'   15.67'   15.67'   15.67'   15.67'   15.67'   15.67'   15.67'   17.81'   17
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457 L458 L459 L460 L461	\$ 50°03'04" E \$ 09°17'34" E \$ 09°17'34" E \$ 79°21'04" W \$ 14°24'15" W \$ 16°37'26" W \$ 50°51'26" W \$ 57°14'43" W \$ 37°34'49" W \$ 47°48'59" W \$ 10°51'24" E \$ 03°59'44" W \$ 17°34'09" W \$ 13°20'30" W \$ 10°58'40" E \$ 58°23'57" W	15.98' 13.81' 10.24' 17.34' 19.24' 17.57' 8.83' 16.00' 20.70' 12.96' 19.79' 14.86' 15.67' 11.72'
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457 L458 L459 L460	\$ 50°03'04" E \$ 09°17'34" E \$ 79°21'04" W \$ 14°24'15" W \$ 16°37'26" W \$ 16°37'26" W \$ 57°14'35" W \$ 37°34'49" W \$ 37°34'49" W \$ 37°34'49" W \$ 17°34'39" W	15.98'   13.81'   10.24'   17.34'   19.24'   17.57'   8.83'   16.00'   38.75'   20.70'   12.96'   19.79'   14.86'   15.67'   15.67'   15.67'   15.67'   15.67'   15.67'   15.67'   15.67'   17.81'   17
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457 L458 L459 L460 L461 L462 L463 L464	\$ 50°03'04" E \$ 09°174" E \$ 79°21'04" W \$ 14'24'15" W \$ 16'37'26' W \$ 16'37'26' W \$ 16'37'26' W \$ 50°132' E \$ 37°34'49" W \$ 17'34'59' W \$ 17'34'59' W \$ 17'34'09' W \$ 17'32' 030' W \$ 15'20'30' W \$ 15'20' W \$ 15'2	15.98' 13.81' 10.24' 17.34' 19.24' 17.57' 8.83' 16.00' 38.75' 20.70' 12.96' 19.79' 14.66' 15.67' 11.72' 21.67' 12.94'
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457 L458 L459 L460 L461 L462 L463	\$ 50°03'04" E \$ 09°17'41" E \$ 79°21'04" W \$ 14'724'15" W \$ 16'37'26' W \$ 16'37'26' W \$ 16'37'26' W \$ 50°13'21" E \$ 37°34'49" W \$ 17'34'59" W \$ 17'24'59" W \$ 17'24'59" W \$ 18'22'50'30" W \$ 10'55'40" E \$ 50°2'35" W \$ 32°2'6'04" E \$ 50°3'02'10" W \$ 38°2'6'02'10" W \$ 38°2'6'02'10" W \$ 38°2'6'02'10" W \$ 18'7'8'02'10" W	15.98' 13.61' 10.24' 17.34' 19.24' 17.35' 16.00' 38.75' 20.70' 12.96' 14.86' 11.72' 21.67' 12.94' 14.22'
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457 L458 L459 L460 L461 L462 L463 L464 L465 L466 L466 L466	\$ 50°03'04" E \$ 0.99"134" E \$ 7.92"104" W \$ 7.92"104" W \$ 14"24"5" W \$ 14"24"5" W \$ 160°52'26" W \$ 60°52'26" W \$ 57"34'49 W \$ 77"34'49 W \$ 70"53'26" W \$ 70"56'40" E \$ 508"46'24" W \$ 8 70"46'24" W \$ 8 70"46'24" W \$ 70"56'20'0" W \$ 70"8'20'0" W \$ 70"8'20'0" W	15.98'   13.81'   10.24'   17.34'   17.34'   19.24'   17.57'   16.00'   18.83'   16.00'   12.96'   19.79'   14.86'   19.79'   14.86'   19.79'   14.86'   19.79'   14.86'   19.79'   1
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457 L458 L459 L460 L461 L462 L463 L464 L465 L465 L466 L467	\$ 50°03'04" E \$ 09°174" E \$ 79°21'04" W \$ 14°24'15" W \$ 14°24'15" W \$ 16°37'26" W \$ N 60°52'26" W \$ N 60°52'26" W \$ 57°14'43" W \$ 37°34'49" W \$ 07°34'49" W \$ 17°34'09" W \$ 17°24'09" W \$ 17°24'09" W \$ 17°26'09" W \$ 18°22'6'04" E \$ 58°02'10" W \$ 18°22'6'04" W	15.98'   13.81'   14.81'   15.98'   17.34'   17.34'   19.24'   17.57'   18.63'   16.00'   19.79'   19.79'   19.79'   19.79'   19.79'   14.86'   15.67'   17.22'   21.67'   12.94'   14.22'   20.00'   14.22'   20.00'   19.79'   14.22'   20.00'   19.79'   19.72'   19.72'   19.72'   19.72'   19.72'   19.72'   19.72'   20.00'   19.79'   1
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457 L458 L459 L460 L461 L462 L463 L464 L465 L466 L467 L466 L467 L468	\$ 50°03'04" E \$ 09°174" E \$ 79°21'04" W \$ 14°24'15" W \$ 14°24'15" W \$ 16'37'26" W \$ N 60'52'28" W \$ N 60'52'28" W \$ 37°34'49" W \$ 37°34'49" W \$ 17°34'09" W \$ 13°23'09" W \$ 13°20'30" W \$ 13°20'30" W \$ 13°20'30" W \$ 22'26'04" E \$ 56°210" W \$ 76°5210" W \$ 76°5210" W \$ 76°5210" W \$ 76°5210" W \$ 76°52'13" W	15.98' 13.81' 17.34' 17.34' 19.24' 17.57' 18.63' 16.00' 12.96' 19.79' 14.86' 15.67' 12.96' 14.22' 20.00' 32.18' 32.18' 32.18' 34.63' 34.75' 35
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457 L458 L460 L461 L462 L463 L464 L465 L465 L466 L467 L468 L469 L469 L470	\$ 50°03'04" E \$ 09°174" E \$ 79°21'04" W \$ 14'724'15" W \$ 16'37'26' W \$ 16'37'26' W \$ 16'37'26' W \$ 57°14'3' W \$ 37°34'49" W \$ 17'34'59" W \$ 17'34'59" W \$ 17'34'09" W \$ 17'34'09" W \$ 17'34'09" W \$ 17'32'030' W \$ 10'58'40' E \$ 58°23'57" W \$ 10'58'40' E \$ 58°23'57" W \$ 10'58'40' E \$ 1	15.98' 13.61' 10.24' 17.34' 17.34' 17.57' 8.83' 16.00' 12.96' 19.79' 14.66' 11.72' 20.00' 21.94' 22.00' 20.91' 32.18' 21.66' 21.66' 33.18' 36.42' 43.11'
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457 L460 L461 L462 L463 L464 L467 L466 L467 L468 L470 L471 L472 L473	\$ 50°03'04" E \$ 09°174" E \$ 79°21'04" W \$ 14'724'15" W \$ 16'37'26' W \$ 16'37'26' W \$ 16'37'26' W \$ 57°14'3' W \$ 37°34'49" W \$ 17'34'59" W \$ 17'34'09" W \$ 10'58'40' E \$ 58°23'57" W \$ 10'58'40' E \$ 58°23'57" W \$ 10'58'40' E \$ 10'58'35' W \$ 10'58'40' E \$ 10	15.98' 13.61' 10.24' 17.34' 17.34' 17.57' 8.83' 16.00' 12.96' 19.79' 14.66' 11.72' 20.00' 21.96' 21.60' 21.
L448 L449 L450 L451 L452 L453 L454 L455 L456 L456 L456 L460 L461 L462 L463 L464 L465 L466 L466 L467 L468 L469 L470 L471 L472 L473	\$ 50°03'04" E \$ 09°174" E \$ 79°21'04" W \$ 14°24'15" W \$ 14°24'15" W \$ 16°37'26" W \$ 16°37'26" W \$ 16°37'26" W \$ 27°34'39' W \$ 27°34'39' W \$ 27°34'39' W \$ 13°23'30' W \$ 13°23'3' W	15.98    13.81    13.81    13.81    13.81    10.24    17.34    19.24    17.37    18.83    18.00    19.24    17.57    18.53    18.00    19.79    19.79    14.86    15.67    19.79    14.86    15.67    16.72    21.67    14.22    20.00    20.91    32.18    14.03    32.18    32.18    33.18    33.18    33.29    3
L448 L449 L450 L451 L452 L454 L455 L454 L455 L456 L466 L461 L462 L466 L467 L468 L467 L468 L470 L471 L472 L473 L474	\$ 50°03'04" E \$ 09°17'41" E \$ 79°21'04" W \$ 14°24'15" W \$ 14°24'15" W \$ 14°24'15" W \$ 16°37'26" W \$ 16°37'26" W \$ 16°37'26" W \$ 27°34'39" W \$ 27°34'39" W \$ 15°32'26" W \$ 15°32'35" W \$ 16°32'4" W \$ 15°32'35" W \$ 16°32'4" W \$ 16°32'4" W \$ 16°32'35" W \$ 16°	15.9e    15.9e    15.9e    15.9e    15.9e    17.34   17.57
L448 L449 L450 L451 L452 L453 L454 L455 L456 L457 L458 L456 L457 L458 L460 L461 L462 L463 L464 L465 L466 L467 L470 L471 L472 L473 L474	\$ 50°03'04" E \$ 0°90'34" E \$ 7°92'104" W \$ 14"24'15" W \$ 16"37'26" W \$ 16"37'26" W \$ 16"37'26" W \$ 16"37'26" W \$ 37"34'39" W \$ 37"34'39" W \$ 15"33'26" W \$ 15"23'20" W \$ 15"20'46" W \$ 1	15.98' 13.81' 17.34' 17.34' 17.57' 8.83' 16.00' 19.79' 19.79' 14.86' 16.67' 12.94' 14.22' 20.00' 32.18' 41.03' 36.42' 41.03' 36.42' 43.11' 29.17' 39.29' 16.70'
_448 _449 _445 _450 _451 _452 _454 _455 _456 _457 _468 _469 _466 _467 _468 _466 _467 _468 _470 _470 _471 _472 _473	\$ 50°03'04" E \$ 09°17'41" E \$ 79°21'04" W \$ 14°24'15" W \$ 14°24'15" W \$ 14°24'15" W \$ 16°37'26" W \$ 16°37'26" W \$ 16°37'26" W \$ 27°34'39" W \$ 27°34'39" W \$ 15°32'26" W \$ 15°32'35" W \$ 16°32'4" W \$ 15°32'35" W \$ 16°32'4" W \$ 16°32'4" W \$ 16°32'35" W \$ 16°	15.9e    15.9e    15.9e    15.9e    15.9e    17.34   17.57

L544	N 80°09'46" W
L545	N 7P42'!7" W
L546	N 7P42'!7" W
L546	N 78°53'56" W
L547	S 09°40'35" W
L549	S 67°55'06" W
L549	S 67°55'06" W
L550	S 76°57'00" W
L551	S 22"06'19" W
L552	S 77°03'50" W
L553	S 25°27'25" E
L555	S 78°43'06" E
L556	S 78°43'06" E
L557	S 69°44'17" E
L558	S 56°32'36" E
L559	S 74°33'06" E
L559	S 74°33'06" E
L550	S 78°33'06" E
L550	S 78°33'06" E
L551	S 69°44'17" E
L552	S 78°33'06" E
L553	S 56°32'36" E
L556	S 19°53'36" E
L556	S 19°53'36" E
L566	S 19°53'36" E
L566	S 19°57'07" W
L566	S 19°53'36" E
L566	S 19°53'36" W
L567	S 79°33'59" W
L568	S 68°20'31" W
L569	S 74°39'35" W
L570	N 67°47'48" W
L571	N 67°47'48" W
L575	N 67°47'48" W
L576	N 70°48'04" W
L577	N 32'15'06" W
L578	S 86°25'34" E
L579	N 68°33'4" E
L579	N 70°46'04" W
L576	N 70°46'04" W
L577	N 32'15'06" W
L578	S 86°25'34" E
L599	N 78°21'46" W
L590	N 78°21'40" W
L591	N 78°21'40" W
L592	N 78°21'21" W
L593	N 78°21'34" W
L594	N 78°21'32" W
L595	N 78°21'44" W
L595	S 26°19'58" W
L599	S 26°19'58" W

LINE TABLE			LINE TABL	
BEARING 5°58'52" W	LENGTH 48.33'	LINE L60I	BEARING S 75°04'04" W	LENGTH I4.II
2°53'42" W	48.33° 37.72'	L602	N 78°16'50" W	28.74
3°52'38" W	30.05'	L603	N 29°24'56" W	31.66
53°53'12" W 50°51'25" W	19.51' 22.98'	L604 L605	S 48°07'19" W N 65°00'00" W	9.43' 5.00'
07°16'13" W	20.95	L606	N 36°17'24" E	24.25
02°16'42" E 3°58'49" E	58.94' 8.10'	L607 L608	N 56°35'39" E N 35°19'16" E	42.80 <sup>1</sup> 30.58 <sup>1</sup>
6°28'36" W	55.02'	L609	S 60°41'00" E	23.58
9°06'37" W	16.22' 61.85'	L6I0	S 60°57'17" E S 68°46'06" E	43.54' 20.07'
SI°57'30" W	18.33'	L612	S 00°00'00" E	5.00
46°41'31" W i7°48'58" W	29.49'	L6I3	N 78°18'49" W S 26°51'43" W	20.25
35°34'19" W	56.72' 25.09'	L614 L615	S 88°18'11" W	20.23'
2°48'58" W	27.79'	L616	S 76°12'36" W	32.27
5°35'49" E 85°37'41" E	105.04' 38.97'	L617	S 45°58'04" W N 87°14'57" W	12.84 <sup>1</sup> 17.59 <sup>1</sup>
5I°00'42" E	48.11	L619	N 27°06'27" E	14.20'
66°33'I4" E 66°45'54" E	37.4I' 22.30'	L620	N 08°55'27" E S 84°33'44" E	10.89 <sup>1</sup> 3.95 <sup>1</sup>
6°30'42" E	45,48	L622	N 33°47'23" W	9,92'
9°36'20" W 37°31'27" W	53.54' 14.18'	L623	S 26°07'28" W S 19°35'33" W	34.03 <sup>1</sup> 30.47 <sup>1</sup>
16°35'41" E	56.77'	L625	S 35°19'20" W	23.04
58°01'45" E 58°56'58" E	30.60' 22.04'	L626 L627	N 80°00'00" W N 26°05'51" E	4.00' 25.00'
4°54'56" E	39.98'	L628	N 18°52'18" E	49.34
55°20'20" E	28.50'	L629	N 29°04'44" E	25.10
6°28'47" E 9°59'03" W	20.48' 31.17'	L630	N 68°45'08" E N 89°17'07" E	15.15'
4°05'25" W	21.56	L632	N 55°16'34" E	34.13'
36°53'22" E	74.29' I5.25'	L633 L634	N 46°53'21" E N 63°22'09" E	15.18' II.40'
55°24'02" E	22.77'	L635	S 20°02'46" W	38.43
52°48'10" E 81°17'40" E	28.26' 3l.76'	L636 L637	S 21°40'21" W S 29°31'06" W	21.33 <sup>1</sup> 37.88 <sup>1</sup>
3°42'23" E	23.52'	L638	S 34°07'57" W	26.32
60°21'25" E 49°41'20" E	33.89' 20.43'	L639	S 87°36'43" W S 77°55'56" W	16.62 <sup>1</sup>
51°27'03" E	23.14	L640 L641	S 89°53'14" W	25.83
57°21'04" E	23.23'	L642	S 82°49'18" W	21.55
71°54'05" E 53°12'59" E	13.44'	L643	N 14°22'01" W N 02°01'16" W	5.69' 80.95'
69°43'I4" E	22.84'	L645	S 09°17'58" W	61.48
14°26'29" E 73°15'08" E	26.7I' 50.38'	L646 L647	S 44°32'27" W S 50°08'39" W	84.57' 68.42'
3°02'30" E	44.12'	2011	1 0 00 00 00 11	00.12
16°37'06" E 05°29'31" W	6.65' 14.06'			
26°18'10" W	16.99'			
6°33'46" W 76°33'12" W	26.65			
33°41'05" W	35.38' 19.72'			
7°22'55" W	9.98'			
'3°04'56" W	16,43' 12.35'	CURVE	RADIUS	LENGTH
10°08'01" W	18.08	CI C2	2905.52' 2905.52'	1860.83' 1434.85'
8°02'52" W 7°24'37" W	25.99' 16.76'	C3	2905,52'	344.51
5°56'04" W	13.44	C4	2905.52'	81.47'
41°33'41" W 28°23'19" W	8.46' I3.37'			
0°09'48" W	19.76			
71°42'17" W '8°53'36" W				
	18.78			
9°48'35" W	17.19' 19.51'			
9°48'35" W	17.19' 19.51' 16.03'			
99°48'35" W '6°57'00" W 67°35'18" W 35°16'27" W	17.19' 19.51' 16.03' 14.88'			
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			CURVE TABLE		
CURVE	RADIUS	LENGTH	CH BEARING	CH LENGTH	DELTA
CI	2905.52	1860.83	S 21°59'40" W	1829.19'	36°41'41"
C2	2905.52	1434.85	S 17°47'40" W	1420.32	28°17'41"
C3	2905,52	344.51	S 35°20'19" W	344.31	6°47'37"
C4	2905.52	81.47'	N 39°32'19" E	81.46'	I°36'23"



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#### LEGEND

BENCHMARK

MEANDER POINT (NO MONUMENT)

CONCRETE MONUMENT (FOUND)
CONCRETE MONUMENT (SET)
IRON PIPE (FOUND)
IRON PIPE (FOUND)
IRON PIPE (SET)
IRON REBAR (FOUND)
IRON REBAR (SET)
CITICAL/TINW WETLAND AREA
WETLANDS AREA





HEREBY STATE THAT TO THE BEST OF MY PROFESSIONAL KNOWLEDGE. INFORMATION. AND BELIEF. THE SURVEY SHOWN HEREON WAS MADE IN ACCORDANCE WITH THE REQUIREMENTS OF THE STANDARDS OF PRACTICE MANUAL FOR SURVEYING IN SOUTH CAROLINA, AND MEETS OR EXCEEDS THE REQUIREMENTS FOR A CLASS "A" SURVEY AS SPECIFIED THEREIN.

F. ELLIOTTE QUINN III SOUTH CAROLINA PROFESSIONAL LAND SURVEYOR LICENSE NO. 10292

WETLAND SURVEY

### OF TRACT A CONTAINING 70.37 AC.

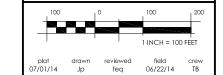
BERKELEY COUNTY, S.C.

PASTIME AMUSEMENT COMPANY



# THOMAS & HUTTON Engineering | Surveying | Planning | GIS | Consulting

682 Johnnie Dodds Blvd., Suite 100 PO Box 1522 Mt. Pleasant, SC 29465-1522 p 843.849.0200 f 843.849.0203



## APPENDIX 3



PO Box B Charleston, SC 29402 103 St. Philip Street (29403)

(843) 727-6800 www.charlestonwater.com **Board of Commissioners** 

Thomas B. Pritchard, Chairman David E. Rivers, Vice Chairman William E. Koopman, Jr., Commissioner Mayor Joseph P. Riley, Jr. (Ex-Officio) Councilmember Dean C. Riegel (Ex-Officio)

Officers

Kin Hill, P.E., Chief Executive Officer
Dorothy Harrison, Chief Administrative Officer
Wesley Ropp, CMA, Chief Financial Officer
Andy Fairey, Chief Operating Officer
Mark Cline, P.E., Capital Projects Officer

8/4/2014

Mr. Stephen Dudash Davis & Floyd, Inc. P.O. Box 61599 Charleston, SC 29419

Re: Water Availability to TMS #263-00-04-001 to serve approximately 80 single family residential units, approximately 560 multi family residential units, 30,000 sf of commercial units, one restaurant

Dear Mr. Dudash,

This letter is to certify our willingness and ability to provide water to the above referenced site in Berkeley County, South Carolina. We currently have a 30" water main in the right-of-way of Hwy. 41 that your property may be served from. Please be advised that it may be necessary to loop the proposed mains into the existing system to achieve adequate pressures. This review does not supplant any other review as required by governing authorities and municipalities. It will of course be a developer responsibility to ensure there are adequate pressures and quantities on this line to serve this site with domestic water/fire flow and not negatively impact the existing developments. Please be advised any extensions or modification to the infrastructure as well as any additional fire protection will be a developer expense. All fees and costs associated with providing water service to this site will be a developer expense. This letter does not reserve capacity in the Charleston Water System infrastructure and it is incumbent upon the developer or his agent to confirm the availability herein granted past 12 months of this correspondence.

The Charleston Water System certifies the availability of service only insofar as its rights allow. Should access to our existing main/mains be denied by appropriate governing authorities, the Charleston Water System will have no other option than to deny service.

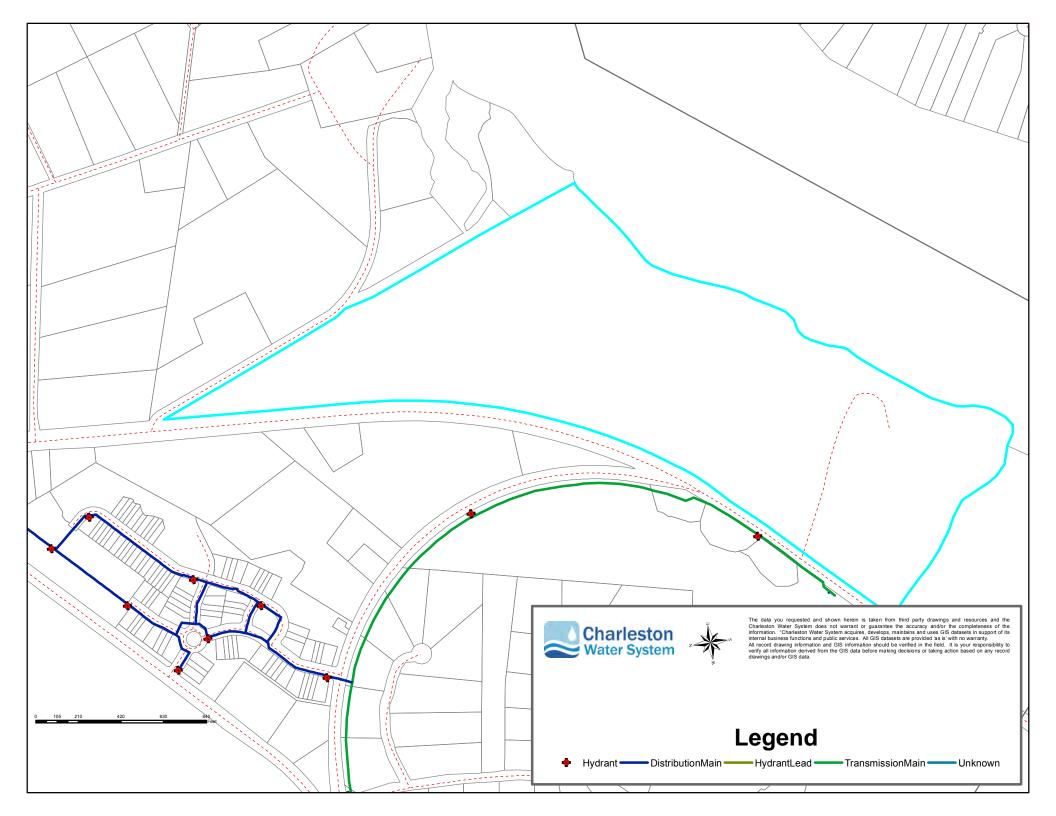
This letter is not to be construed as a letter of acceptance for operation and maintenance from the Department of Health and Environmental Control.

If there are any questions pertaining to this letter, please do not hesitate to call on me at (843) 727-6870.

Sincerely,

Cheryl L. Boyle Engineering Assistant Charleston Water System

cc: file





PO Box B Charleston, SC 29402 103 St. Philip Street (29403)

(843) 727-6800 www.charlestonwater.com **Board of Commissioners** 

Thomas B. Pritchard, Chairman David E. Rivers, Vice Chairman William E. Koopman, Jr., Commissioner Mayor Joseph P. Riley, Jr. (Ex-Officio) Councilmember Dean C. Riegel (Ex-Officio)

Officers

Kin Hill, P.E., Chief Executive Officer Dorothy Harrison, Chief Administrative Officer Wesley Ropp, CMA, Chief Financial Officer Andy Fairey, Chief Operating Officer Mark Cline, P.E., Capital Projects Officer

8/4/2014

Mr. Stephen Dudash Davis & Floyd, Inc. P.O. Box 61599 Charleston, SC 29419

Re: Sewer Availability to TMS #263-00-04-001 to serve approximately 80 single family residential units, approximately 560 multi family residential units, 30,000 sf of commercial units, one restaurant

Dear Mr. Dudash,

This letter is to certify our willingness and ability to provide wastewater collection service to the above referenced site in Berkeley County, South Carolina. Wastewater collection service to this site may be made available via an extension of the existing 18" gravity main going to pump station 171, located on TMS#263-16-01-067, in accordance with CWS Approach Main Policy S88001 available on our website. Any subdividing of the subject property subsequent to this correspondence will require a review process of the civil engineering plans to ensure compliance with the Charleston Water System minimum standards. Any extensions and/or modifications to the infrastructure to serve this site will be a developer expense. Please be advised that wastewater impact fees, wastewater tap fees, change-in-use fees, and/or cost to extend fees will be due prior to connection of any Charleston Water System's sewer system. This letter does not reserve capacity in the Charleston Water System infrastructure and it is incumbent upon the developer or his agent to confirm the availability herein granted past 12 months of this correspondence.

The Charleston Water System certifies the availability of service only insofar as its rights allow. Should access to our existing sewer main/mains be denied by appropriate governing authorities, the Charleston Water System will have no other option than to deny service.

This letter is not to be construed as a letter of acceptance for operation and maintenance from the Department of Health and Environmental Control.

If there are any questions pertaining to this letter, please do not hesitate to call on me at (843) 727-6870.

Sincerely,

Cheryl L. Boyle Engineering Assistant Charleston Water System

cc: file

